

# Regional Technical Seminar

## Short Circuit Design Considerations

Transformer Regional Technical Seminar

Minneapolis, MN

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waukesha  
a prolec ge company



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## Principal Design Engineer

Yuriy joined Prolec GE Waukesha in January 2006, bringing with him 29 years of experience in transformer design. He works out of the Waukesha facility and has designed all types of transformers up to 1150kV, 1000 MVA.

Yuriy holds a Master of Science Degree in Electrical Engineering from Ukrainian University of Engineering.



# Agenda

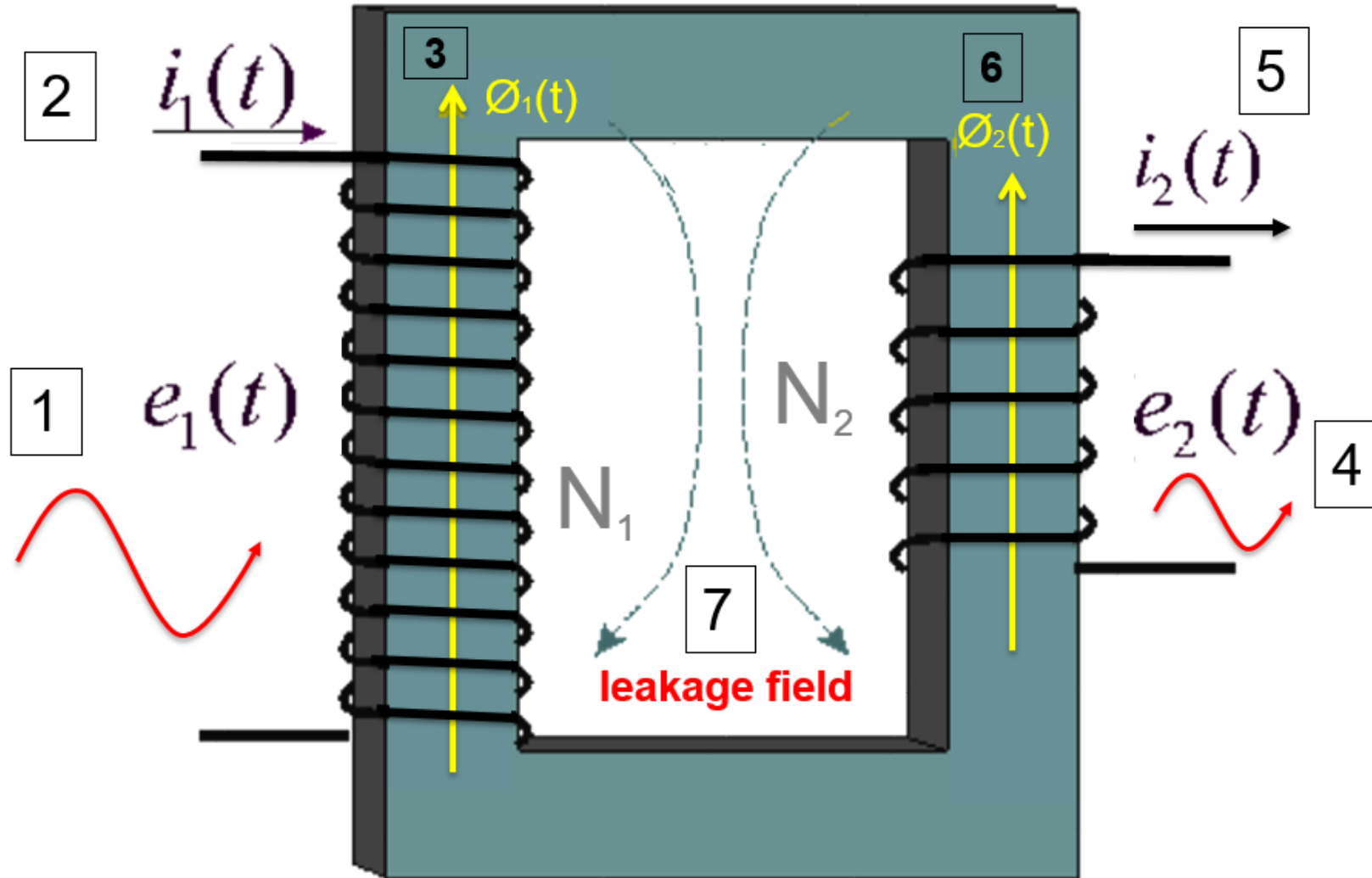
- Review transformers: How they work (textbook vs reality)
- Visualize relationship between Current and Magnetic Forces
- Understand fault current from time  $t = 0$  to  $t = ?$
- Understand formulas and variables to calculate short circuit currents
- Discuss fault types
- Calculation Example: Calculate short circuit amps
- Get a mental picture of magnetic forces acting within a transformer resulting from short circuit



## Part 1 – Transformer Basics:

- How they work
- How they are actually built

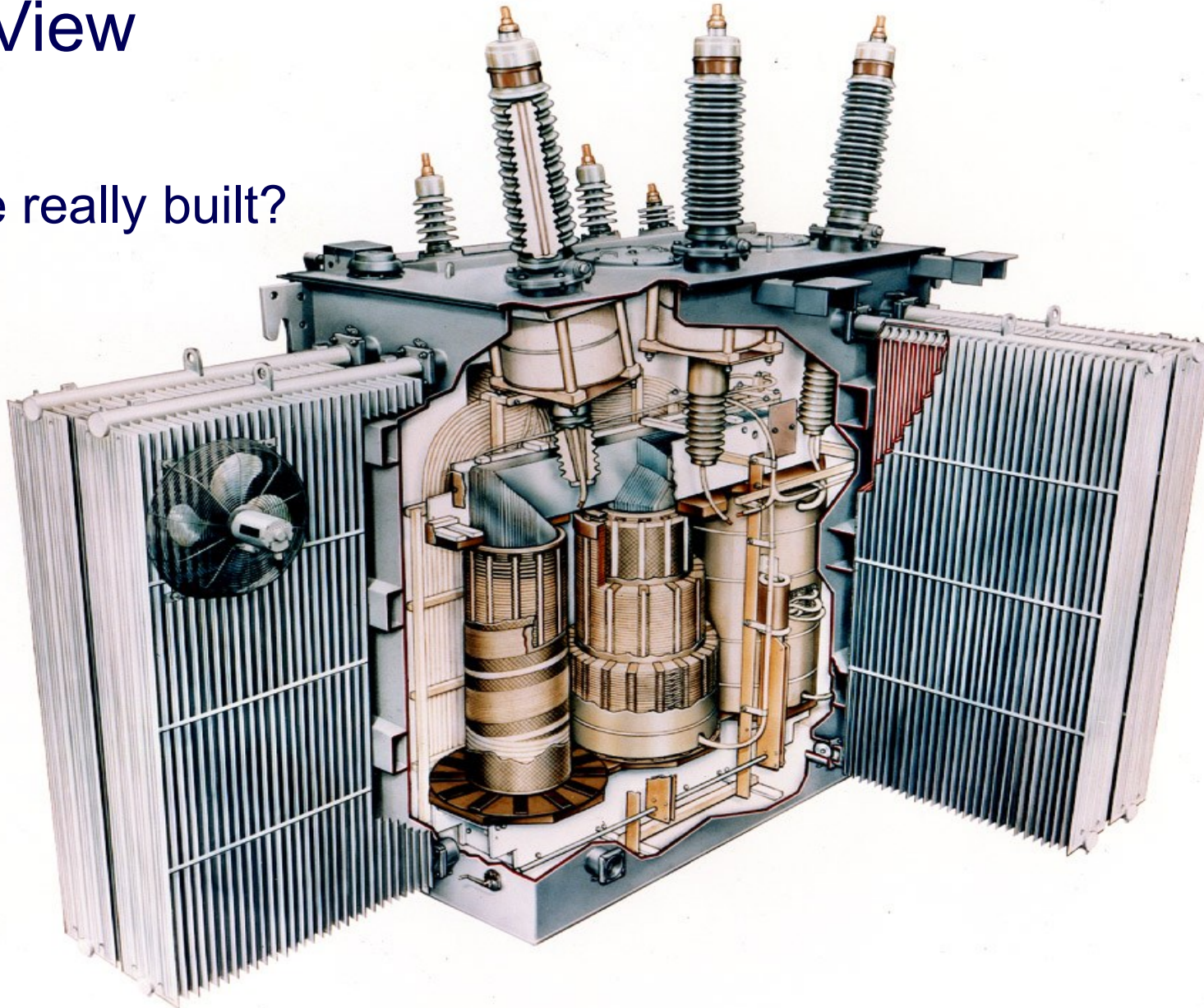
# Textbook Transformer (step by step)





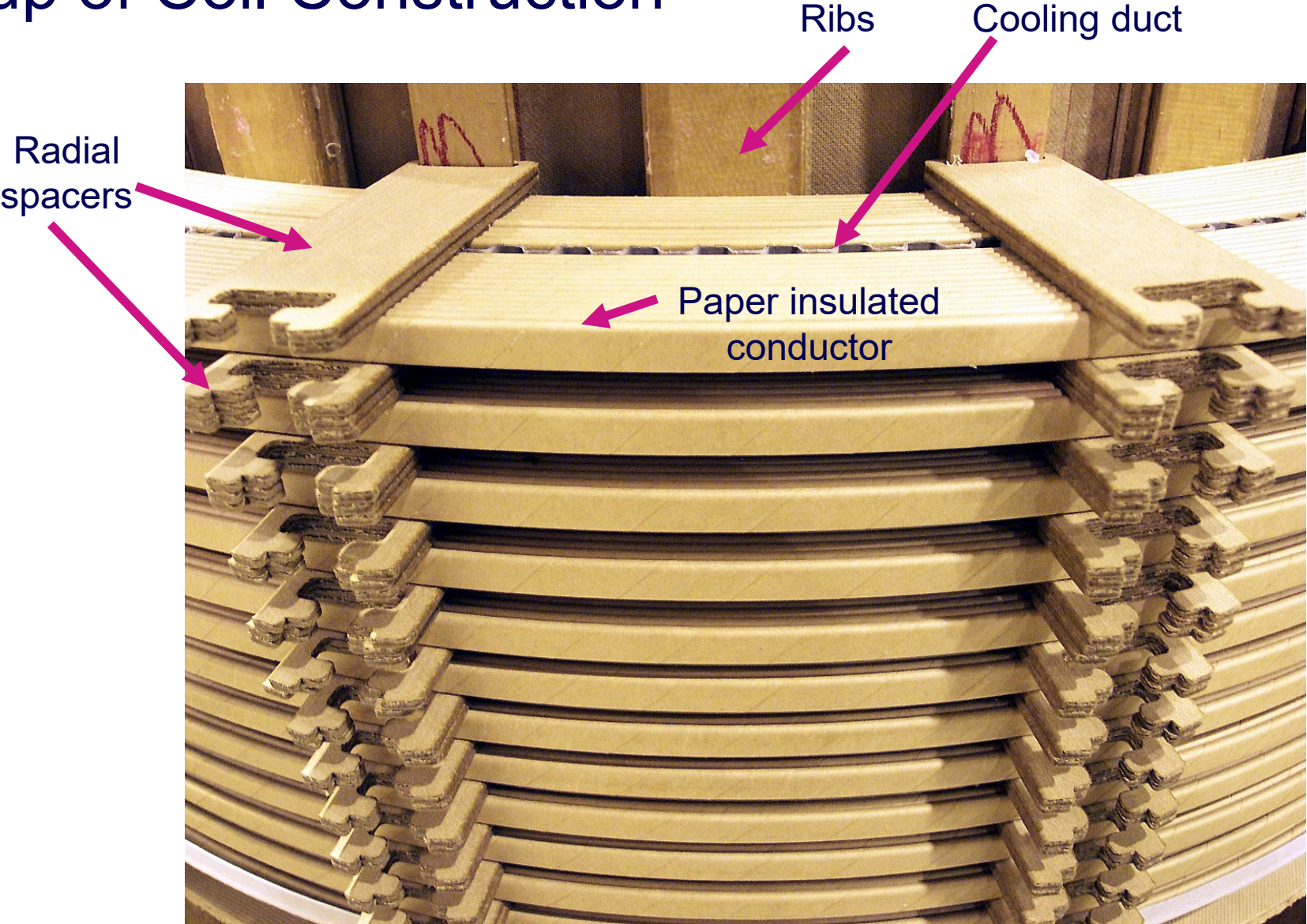
# Cutaway View

How they are really built?





# Close up of Coil Construction

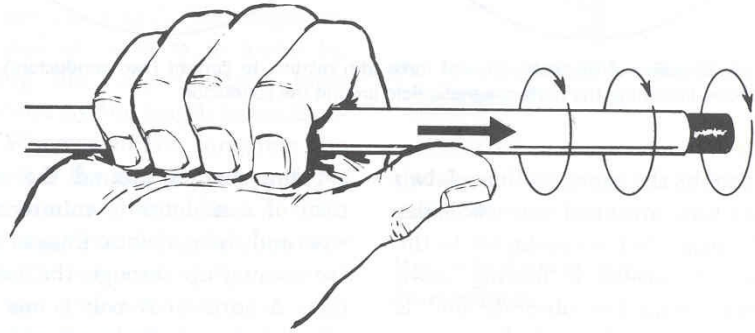


## Part 2 – Transformer Basics:

- Fundamentals of Magnetics and Forces
- Magnetic Fields Around Conductors
- Forces That Result



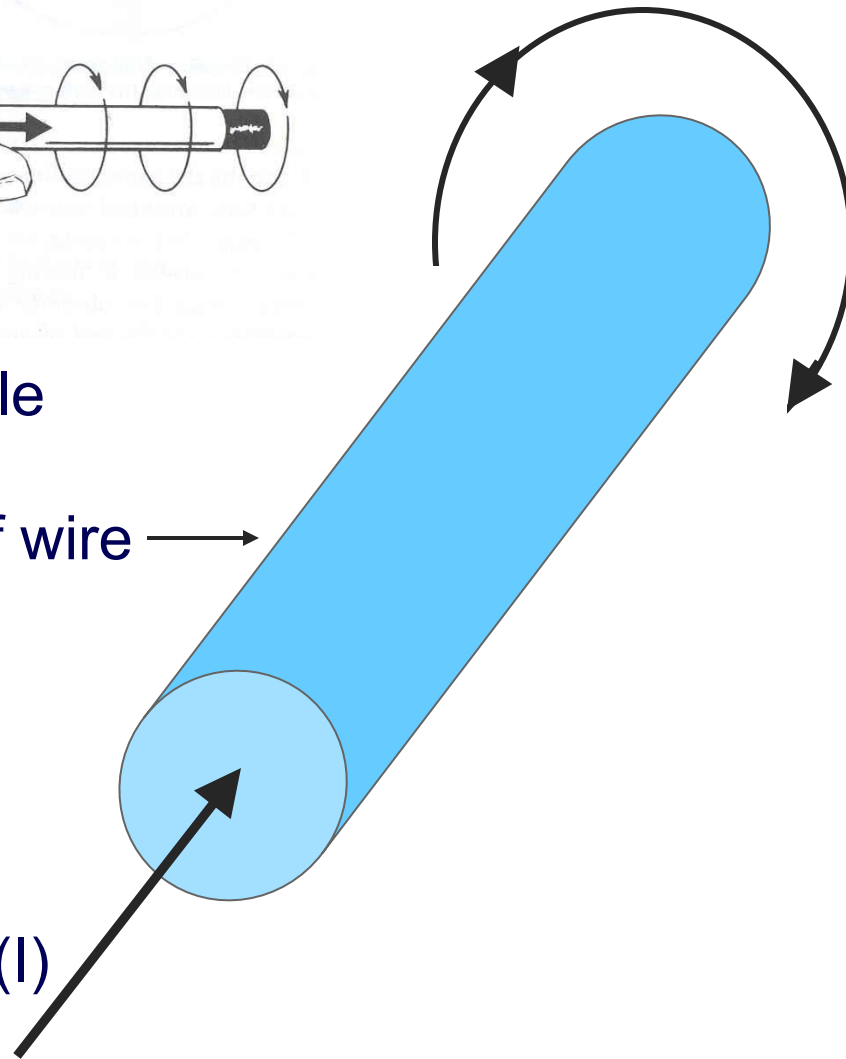
# Current & Magnetic Field Relationships



Right hand rule

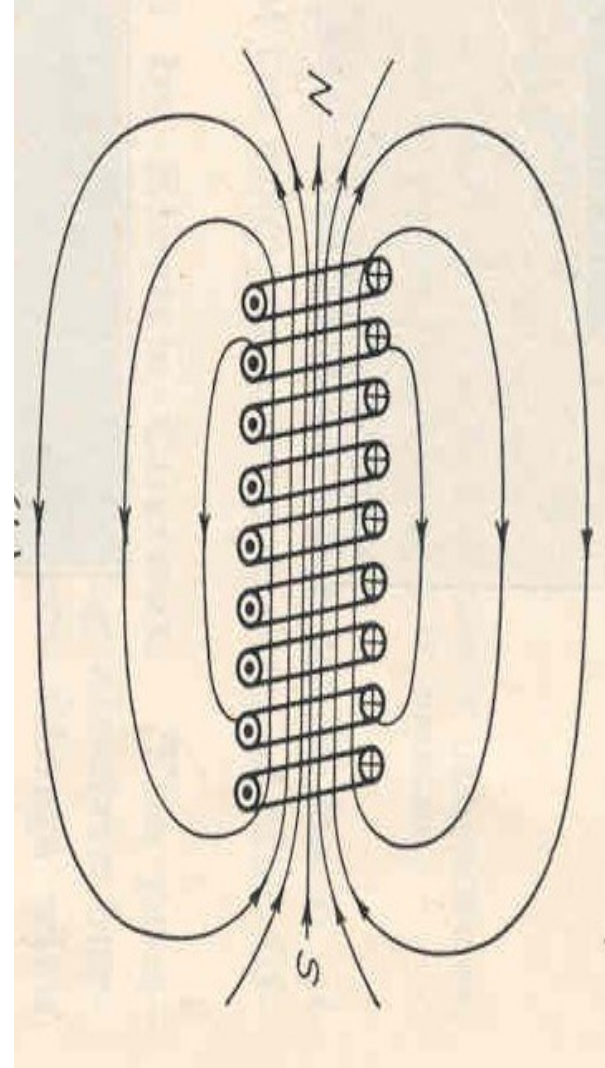
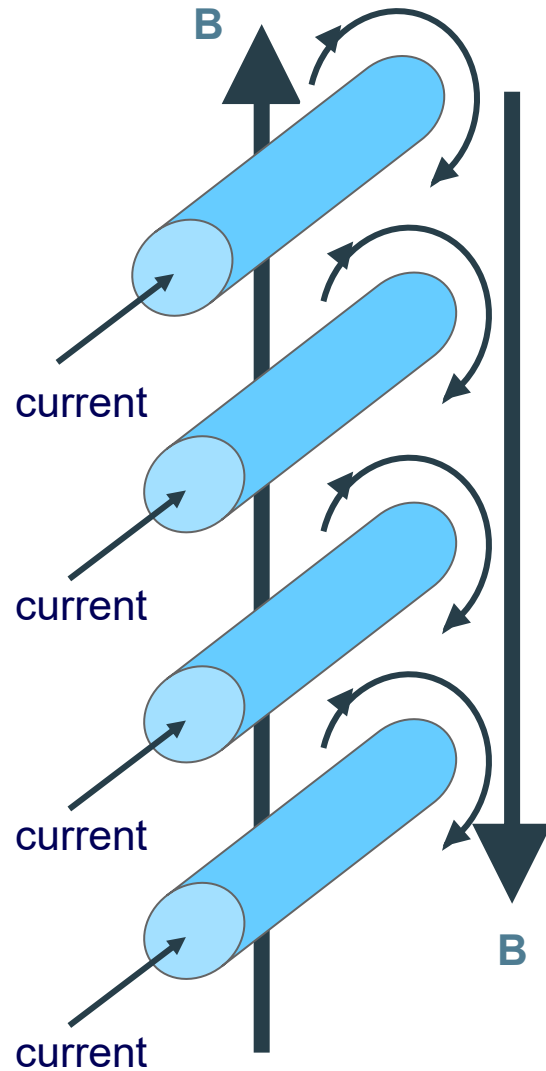
Consider a section of wire →

Current Flow (I) →



resulting  
magnetic  
field direction  
(CW)

# Effect of Many Turns

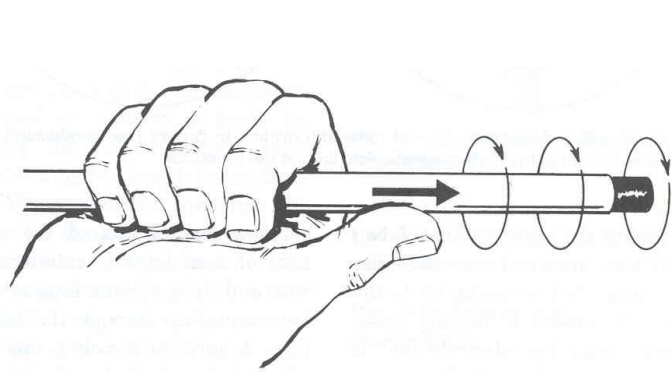


- Fields at inner/outer edges add together.
- One uniform magnetic path results
- Magnetic field (B) intensifies with # turns (N) or the current (I).

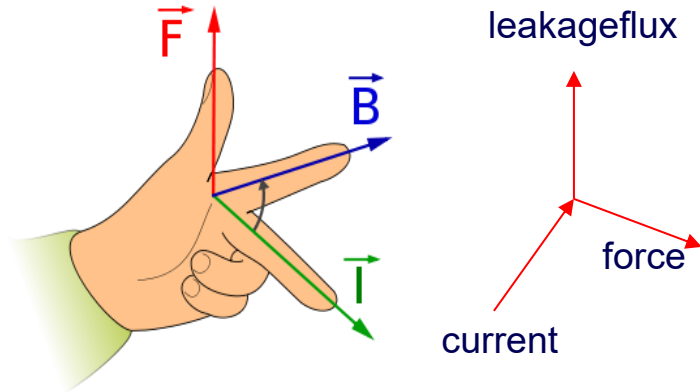
$$B \propto NI$$



# Leakage Field / Current / Force Relationships



Right hand rule



Left hand rule

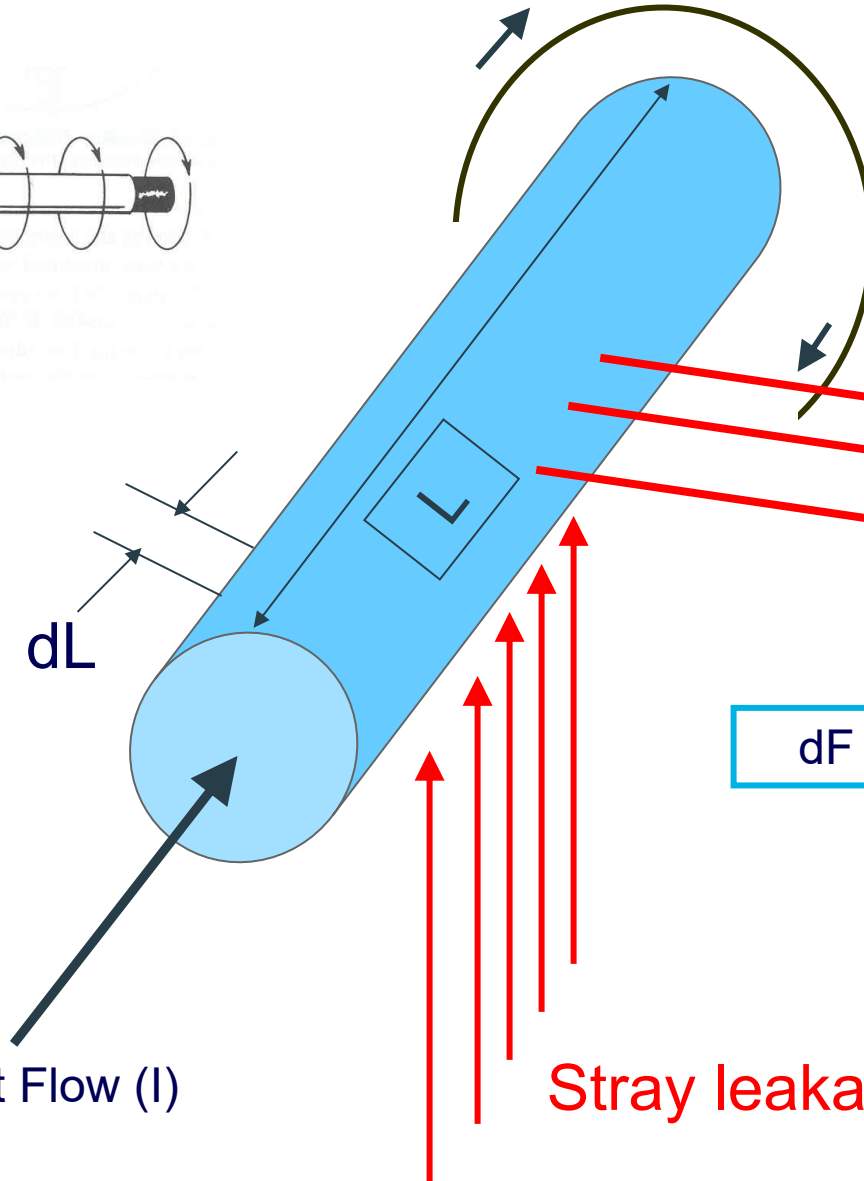
leakage flux

current

force

Current Flow (I)

dL



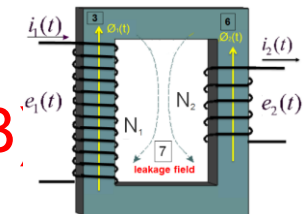
resulting magnetic field direction (CW)

**F**

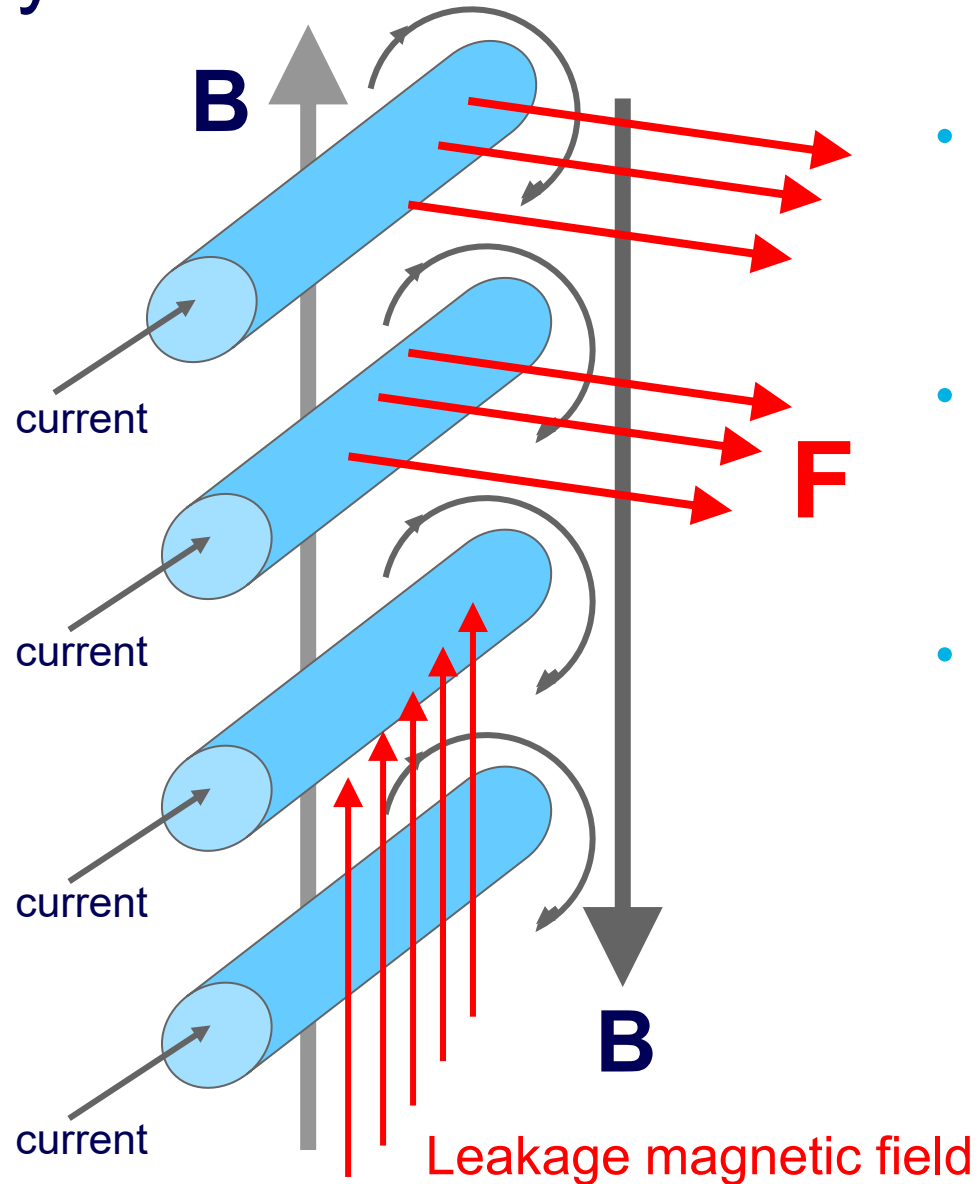
Resulting Force Direction

$$dF = I \times B \, dL$$

Stray leakage field (B)



# Effect of Many Turns



- Fields at inner/outer edges add together
- One uniform magnetic path results
- Magnetic Forces (F) intensifies with # turns (N)

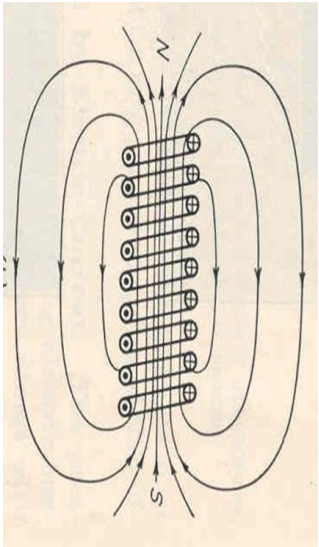
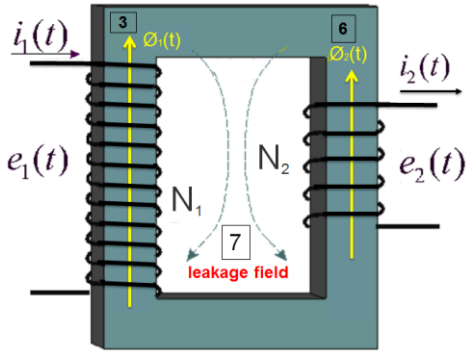
$$B \propto NI$$

$$dF = N \times I B dL$$

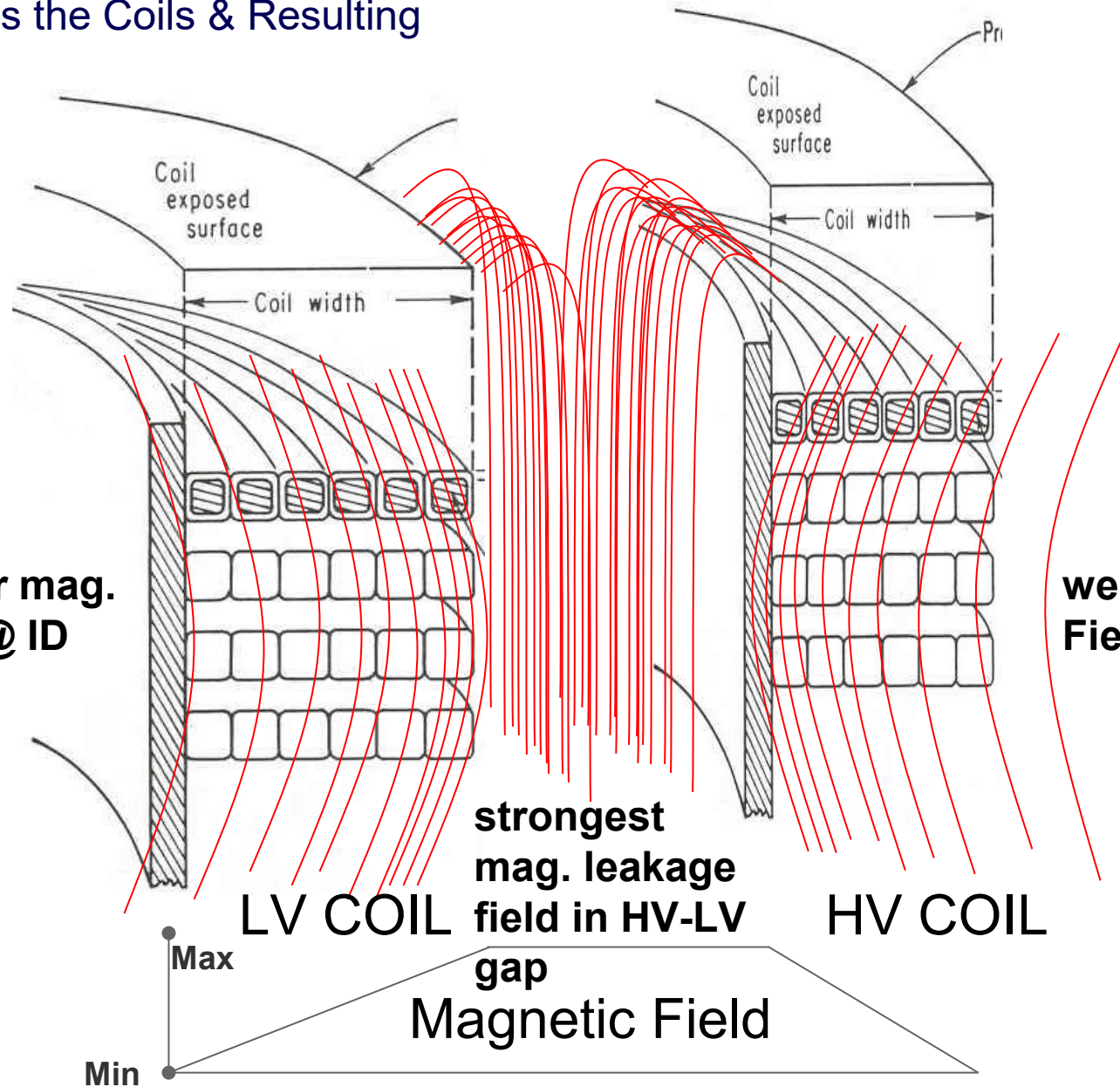
$$F \propto (NI)^2$$



# Magnetic "Leakage" Field Across the Coils & Resulting Forces

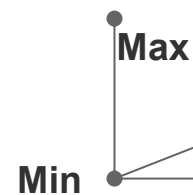


**weaker mag. Field @ ID**

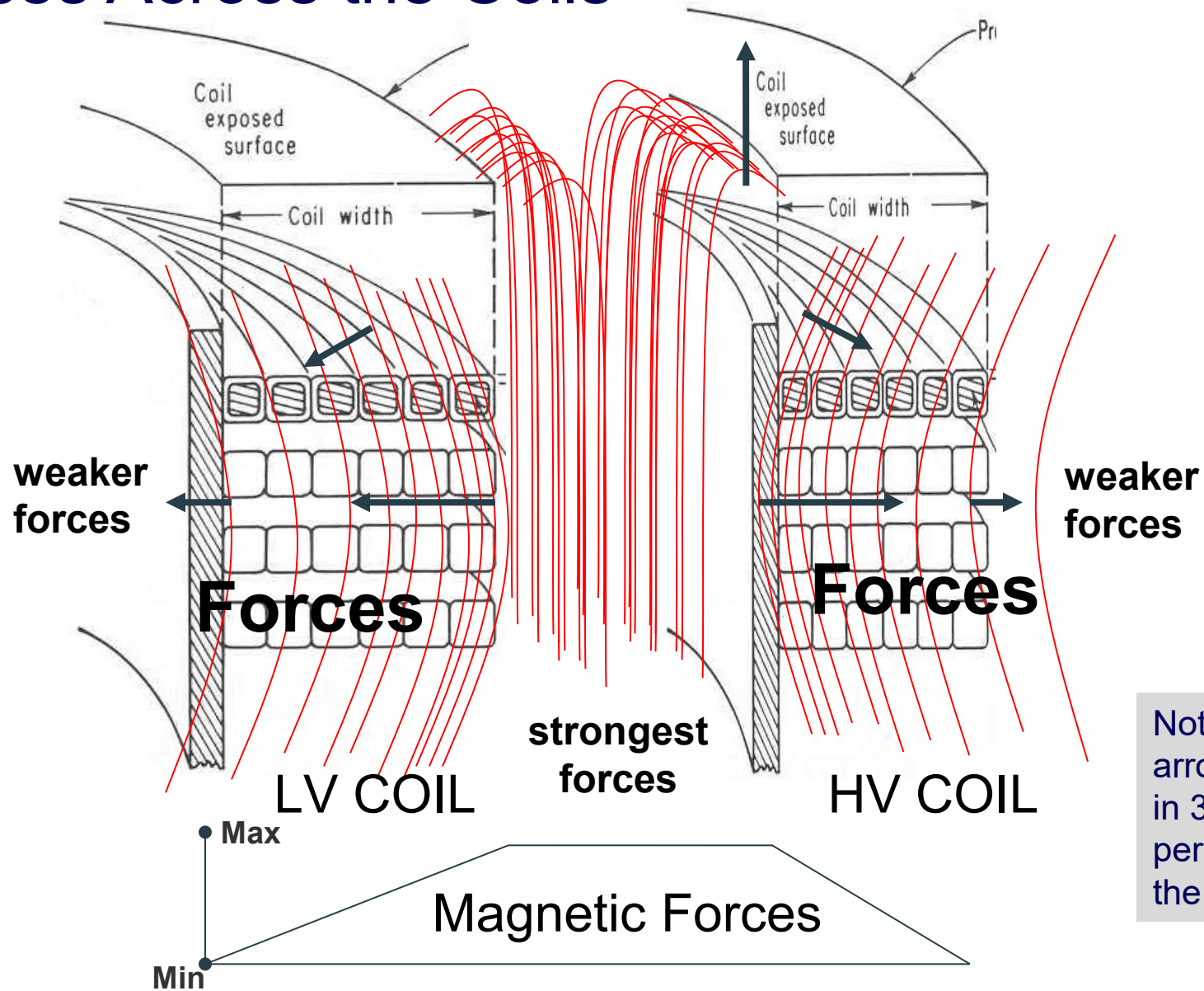
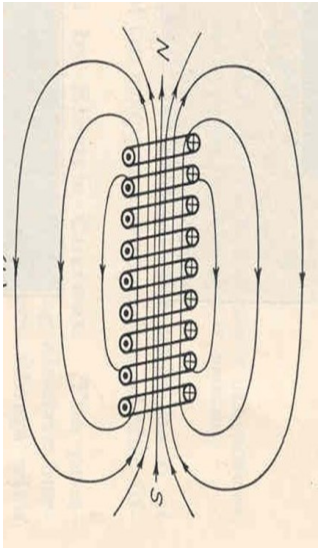
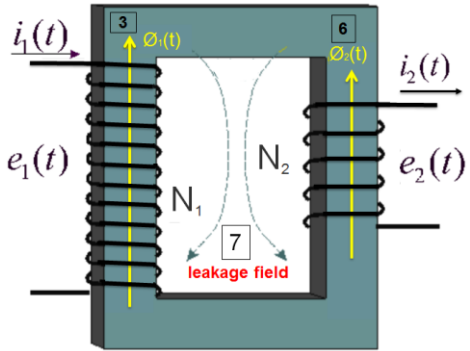


**weaker mag. Field @ OD**

**strongest mag. leakage field in HV-LV gap**  
**Magnetic Field**



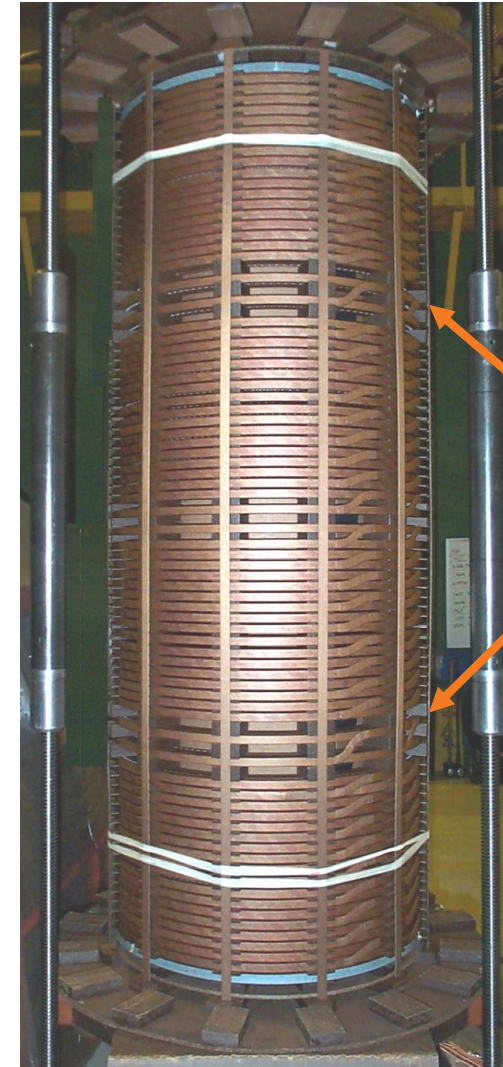
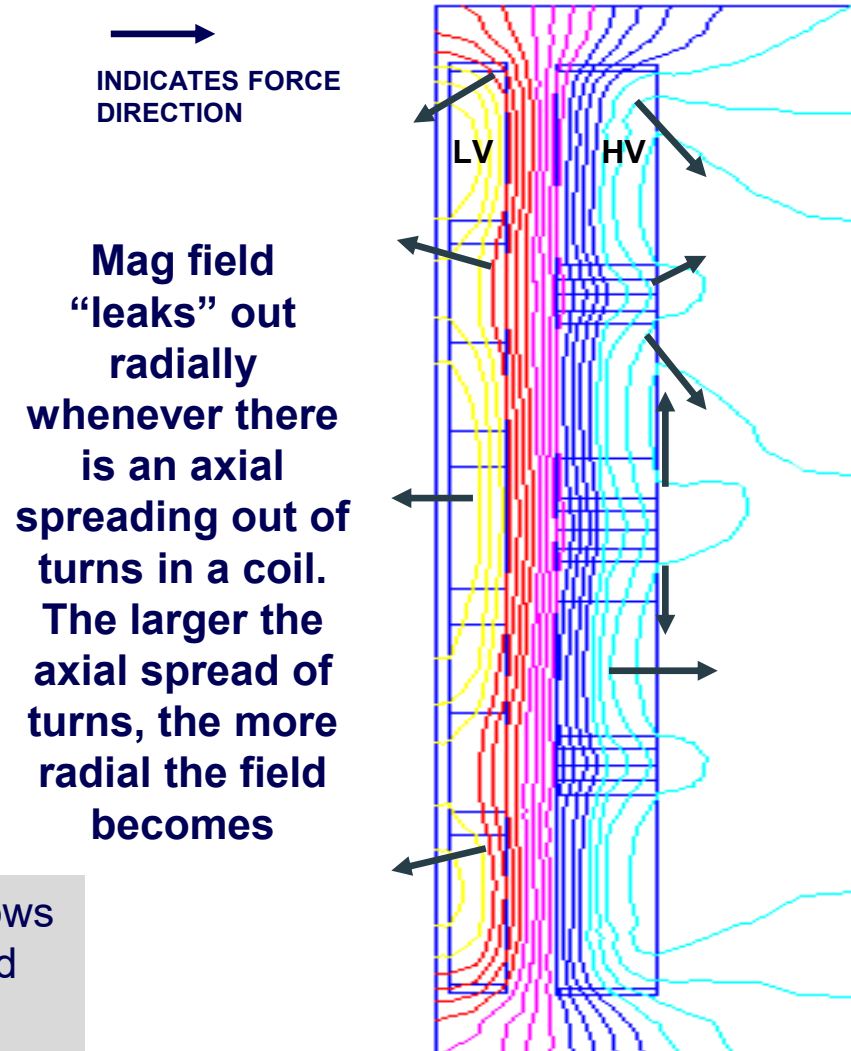
# Magnetic Forces Across the Coils



Note: The force arrows are acting in 3-D and perpendicular to the mag fields



# Pictorial of actual FEA field plots



Axial  
locations  
of where  
HV DETC  
taps are  
located

Note: The force arrows  
are acting in 3-D and  
perpendicular to the  
mag fields

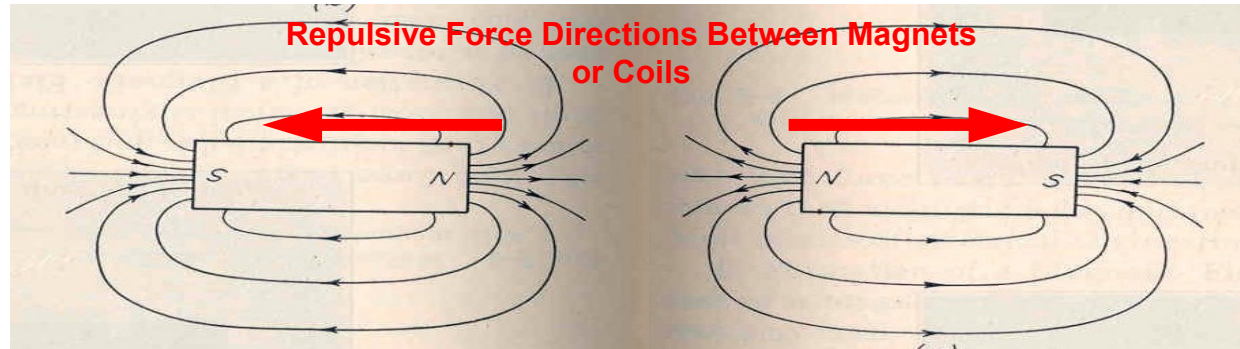
Finite Element Analysis of  
Leakage Field Between Coils

# Summary of what we discussed so far...

- Magnetic forces are produced whenever
  - You have current flowing thru a conductor, and
  - A leakage magnetic field also passes thru the conductor.
  - Resulting forces have a direction of 90 degrees to the direction of current through the conductor versus the direction of the leakage magnetic field around the conductor (left hand rule)
  - The leakage magnetic fields can pass thru conductors at any angle (3 dimensional)
  - Forces then are also 3 dimensional in nature

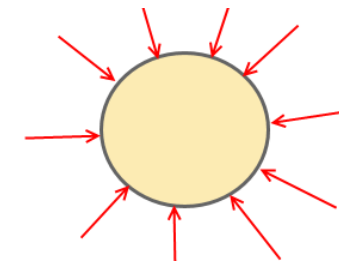
# Magnetic Forces

- A net magnetic force also results between two coils (i.e. HV to LV), because the two coils are essentially two huge electro-magnets that repel each other.

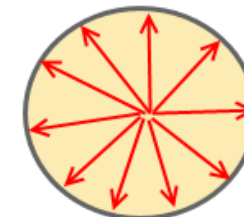


Summative force between these coils could be millions of pounds

- The inner coil experiences net inward radial “crushing” compressive forces
- The outer coil experiences net outward radial expanding type forces



LV coil



HV coil



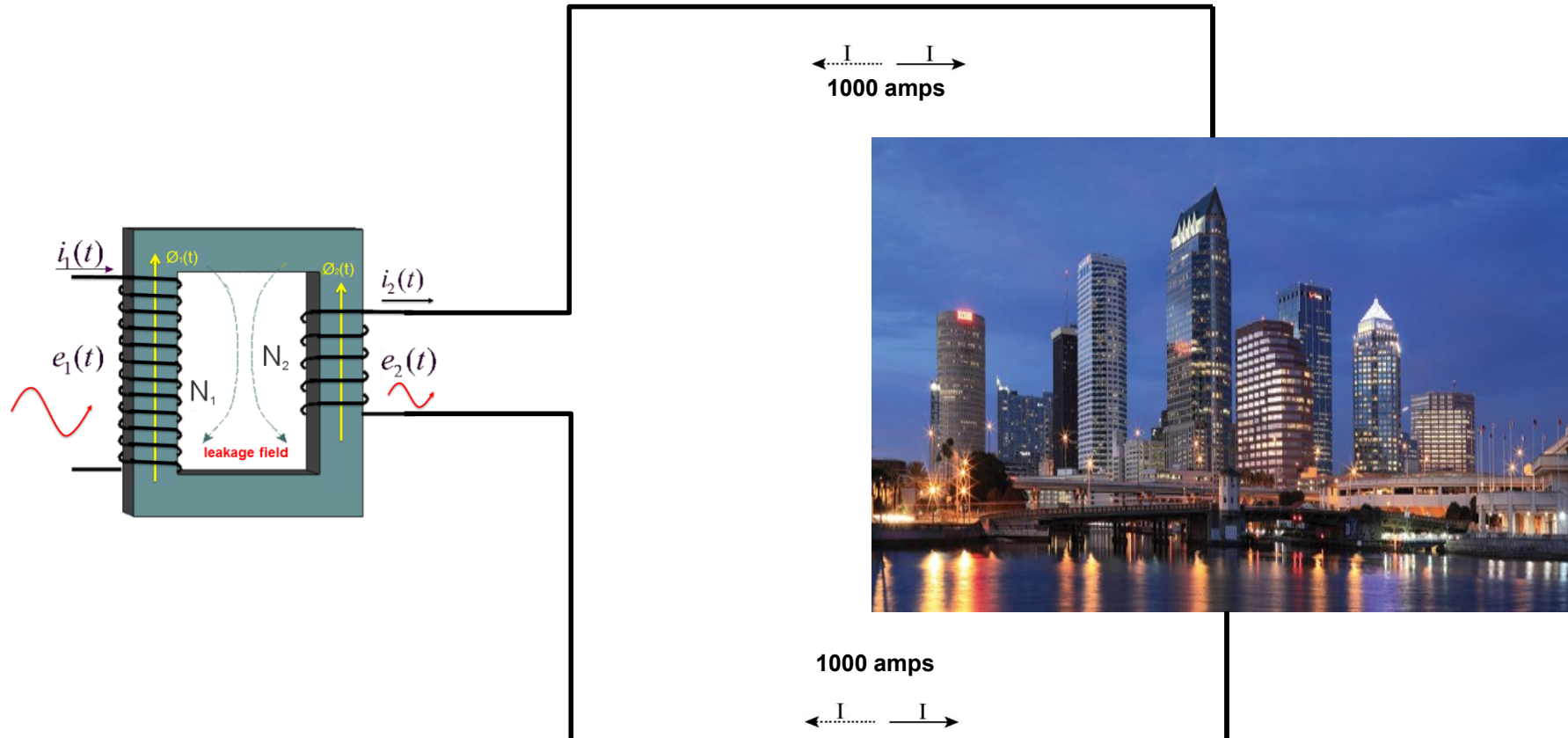
## Part 3 – Short Circuits (Faults):

- What are they?
- How do they happen?
- What do they do to my transformer?

# Normal Transformer Operation

## Normal Circuit

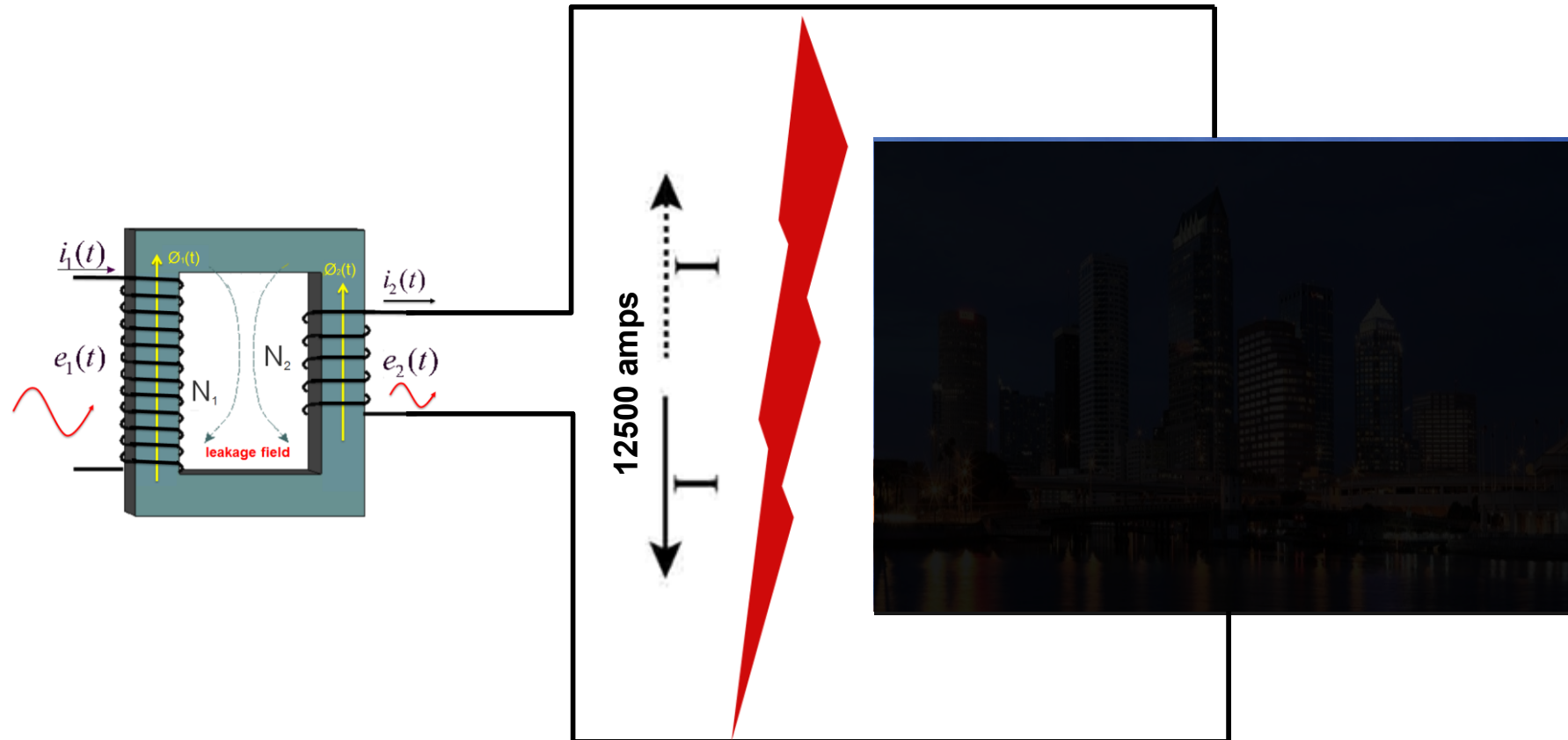
- An AC source supplies power to a given load (i.e. a city). A complete circuit has a source, with power entering a load and returning to the source. Amount of current that flows is directly related to the load on the transformer.



# What is a Fault?

## System Fault

- An un-intended “electrical connection” made between two energized components having different voltage potentials.
- Results in some (or all) of the current bypassing the intended load.
- Currents are typically very high due to low “fault impedance”





# Types of Faults (and how they happen)

## Basic Types of Faults in Power Systems

- Line-to-Ground (Most Common)
  - One or more conductors make “electrical” contact to ground
  - Example: Wildlife or Lightning. A lightning strike hits a line, then causes a flashover. The stroke between the line and ground causes ionization of the air (a conductive channel path to ground).



Lightning can reach 100 million to 1 billion volts, and generate up to a billion watts of power

# Types of Faults (*cont.*)

## Basic Types of Faults in Power Systems

- Line-to-Line
  - Two different phases come into direct or indirect contact with each other
  - Example: A bird with a large wingspan touches two conductors simultaneously and creates a conductive path between the two lines



# Types of Faults (*cont.*)

## Basic Types of Faults in Power Systems

- Double Line-to-ground
- Three Phase (least common)
  - Similar to Line-to-Line but when all three phases make contact with each other
  - Example: A falling tree on a transmission line creates a conductive path between all 3 lines and to ground





# Designing For Short Circuit

Section 7 of IEEE C57.12.00 addresses design requirements for short circuit

- Fault current magnitudes and their behavior over time (time durations, wave shapes, etc).
- Temperature limits of winding conductor after a fault
- Power system impedance that may be used to help limit fault current
- Short circuit test methods and how to analyze, inspect, etc.

# Example of How to Calculate SC Current

C57.12.00 Section 7 defines both symmetrical and asymmetrical current

## Symmetrical Current

$$I_{SC} = \frac{I_R}{Z_T + Z_S}$$

- $I_{sc}$  – symmetrical SC Current (A, rms)
- $I_r$  – rated current (A, rms)
- $Z_t$  – transformer impedance for same voltage tap and MVA as rated current ( $I_r$ )
- $Z_s$  – system impedance in per unit on the same MVA base for rated current ( $I_r$ )

## Asymmetrical Current

$$I_{SC}(pk\ asym) = K I_{SC}$$

$$K = \left\{ 1 + \left[ e^{-\left(\phi + \frac{\pi}{2}\right)\frac{r}{x}} \right] \sin \phi \right\} \sqrt{2}$$

$\phi$  is arc tan ( $x/r$ ) (radians)

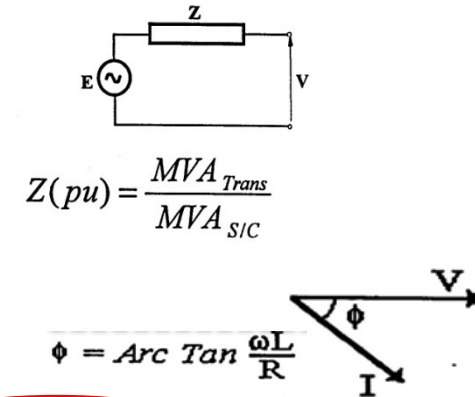
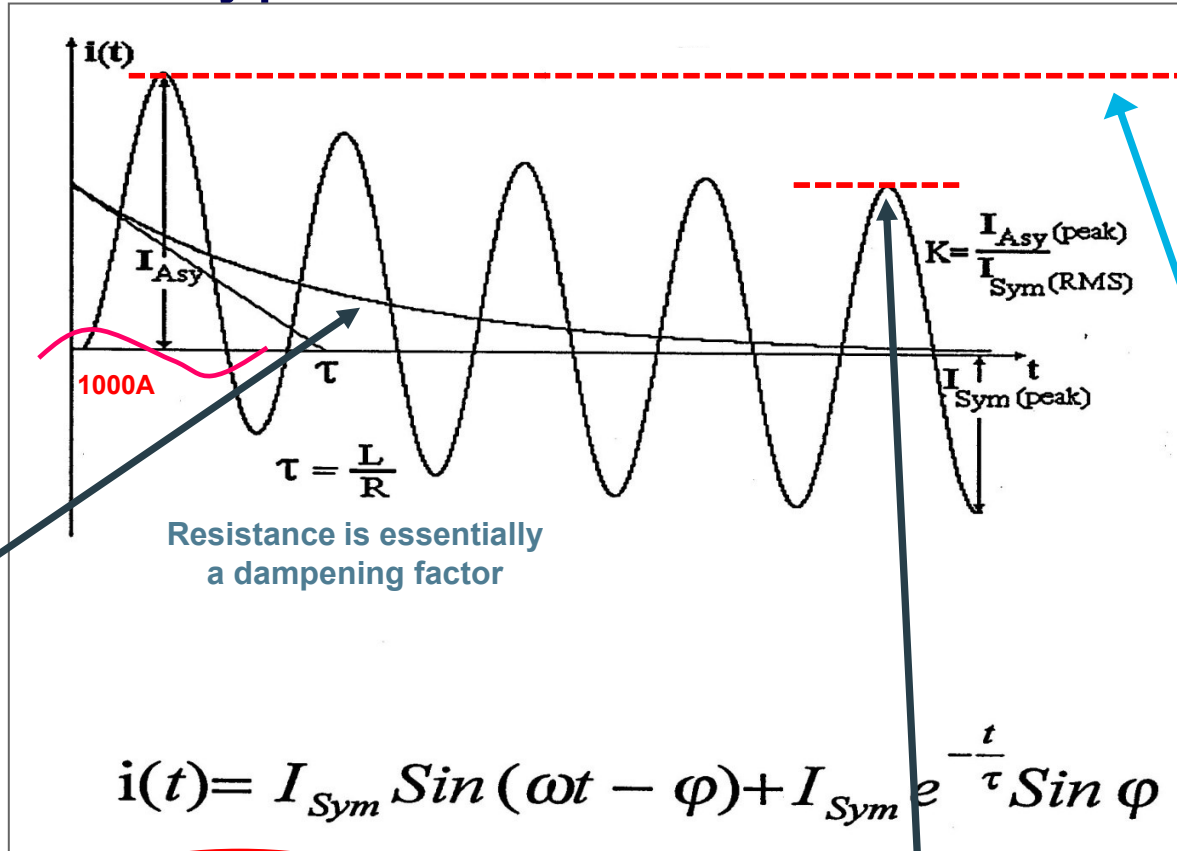
$e$  is the base of natural logarithm

$x/r$  is the ratio of effective ac reactance to resistance, both in ohms

# Waveform of Typical Fault Current Over Time

(Symmetrical and Asymmetrical)

The fault current within a transformer will follow this typical exponential decay



**Asymmetrical (Peak) current**

$$i(t) = I_{Sym} \sin(\omega t - \phi) + I_{Sym} e^{-\frac{t}{\tau}} \sin \phi$$

**Symmetrical (RMS) current**

$$I_{SC} = \frac{I_R}{Z_T + Z_S^*} \quad \text{OR} \quad I_{SC} = \frac{100}{\%Z} \times I_R$$

$$I_{SC}(\text{peak asym}) = K I_{SC} \text{ where}$$

$$K = \left\{ 1 + \epsilon^{-\left(\phi + \frac{\pi}{2}\right) \frac{r}{x}} \sin \phi \right\} \sqrt{2}, \text{ per unit}$$

$$\phi = \arctan \frac{x}{r}, \text{ radians}$$

Say Z were to be 8.0%, then:  
Isc would be 12.5x normal rated current

# Different Parts of the Formulas...

**ASSYM: MECHANICAL DAMAGE**

$e^{-t/\tau}$

The fault current entering a transformer will follow this typical exponential decay

$\phi = \text{Arc Tan } \frac{\omega L}{R}$

**4** Symmetrical

$K = \frac{I_{Asy}(\text{peak})}{I_{Sym}(\text{RMS})}$  **1**

**RATED AMPS**

$\tau = \frac{L}{R}$

Resistance is essentially a dampening factor

**TO FIND ANY POINT IN THE TIMELINE**

**4** Symmetrical

**DECAY PATTERN** **2** **3**

**Asymmetrical (Peak) current**

$I_{SC}(\text{peak asym}) = KI_{SC}$  where **CONVERT RMS TO PEAK**

$K = 1 + \epsilon \left[ \sin\left(\phi + \frac{\pi}{2}\right) e^{-\frac{t}{\tau}} \right] \sqrt{2}$ , per unit

**OFFSET VALUE MAINLY AFFECTED BY X/R**

$\phi = \arctan \frac{x}{r}$ , radians **WORSE CASE AT V=0**

$\frac{1}{\tau} = R/L$

$Z_S = \frac{MVA_{Trans}}{MVA_{SIC}}$

$\tau = X/R$

**THIS FORMULA TAKES YOU RIGHT TO FIRST ASYMMETRICAL PEAK! POINT A**

**K RANGES  $\approx 1.5 - 2.83 \times I_{SC}$**



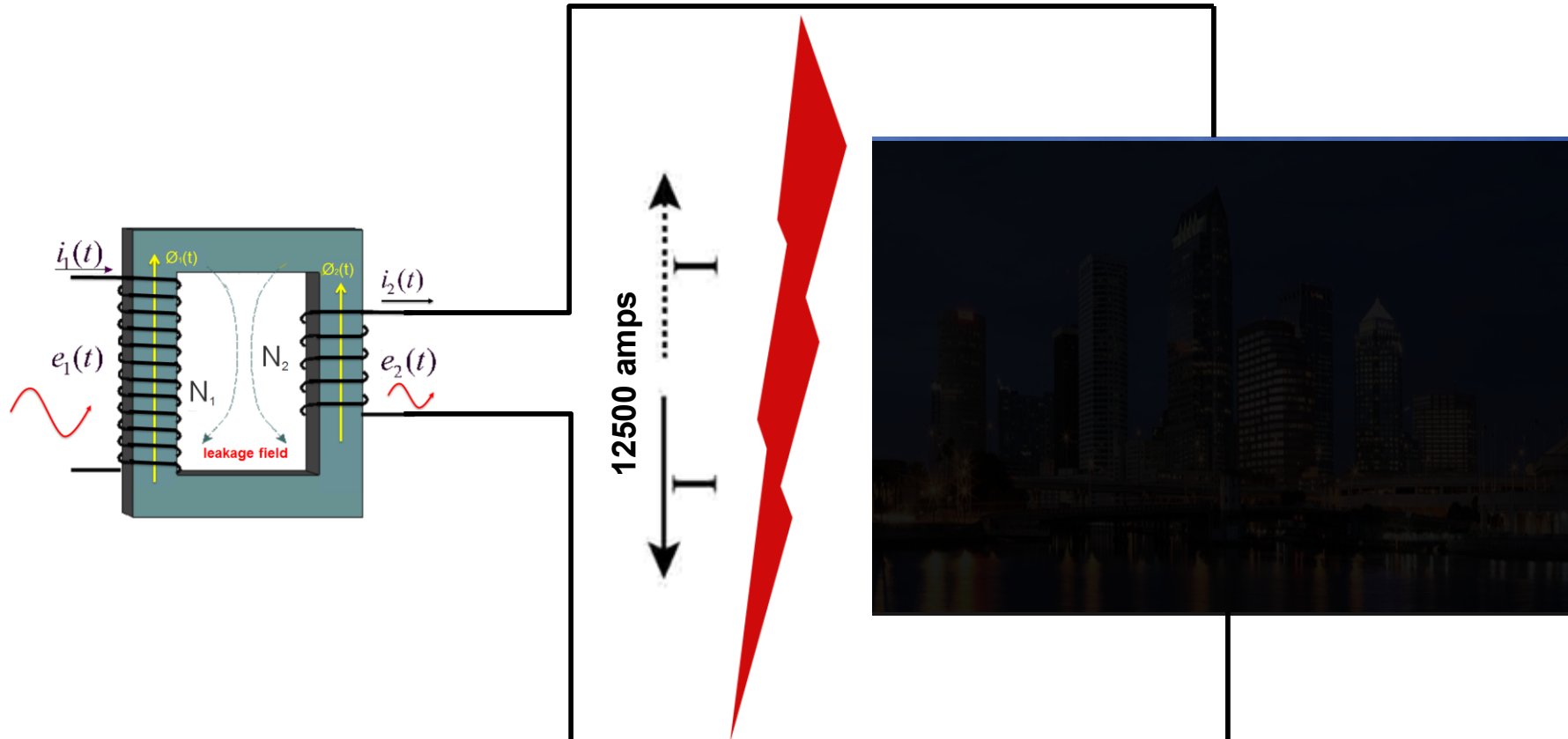
## Part 4 – Visualization of the Magnetic Forces:

- Axial Forces on Winding Conductors (and other components)
- Radial Forces on Winding Conductors
- Combination of Axial/Radial Forces

# Back to our Fault Condition...

## System Fault

- An un-intended “electrical connection” made between two energized components having different voltage potentials.
- Results in some (or all) of the current bypassing the intended load.
- Currents are typically very high due to low “fault impedance”



# Once the Fault Occurs...

- The transformer must source the current to feed the fault
- Very high currents (much higher than rated current) begin to flow in the transformer windings
- Very high temperatures can be generated in the winding conductors and paper insulation resulting from the high currents that flow.
- Very high magnetic forces can be generated within windings, leads, supporting structures and insulation systems.

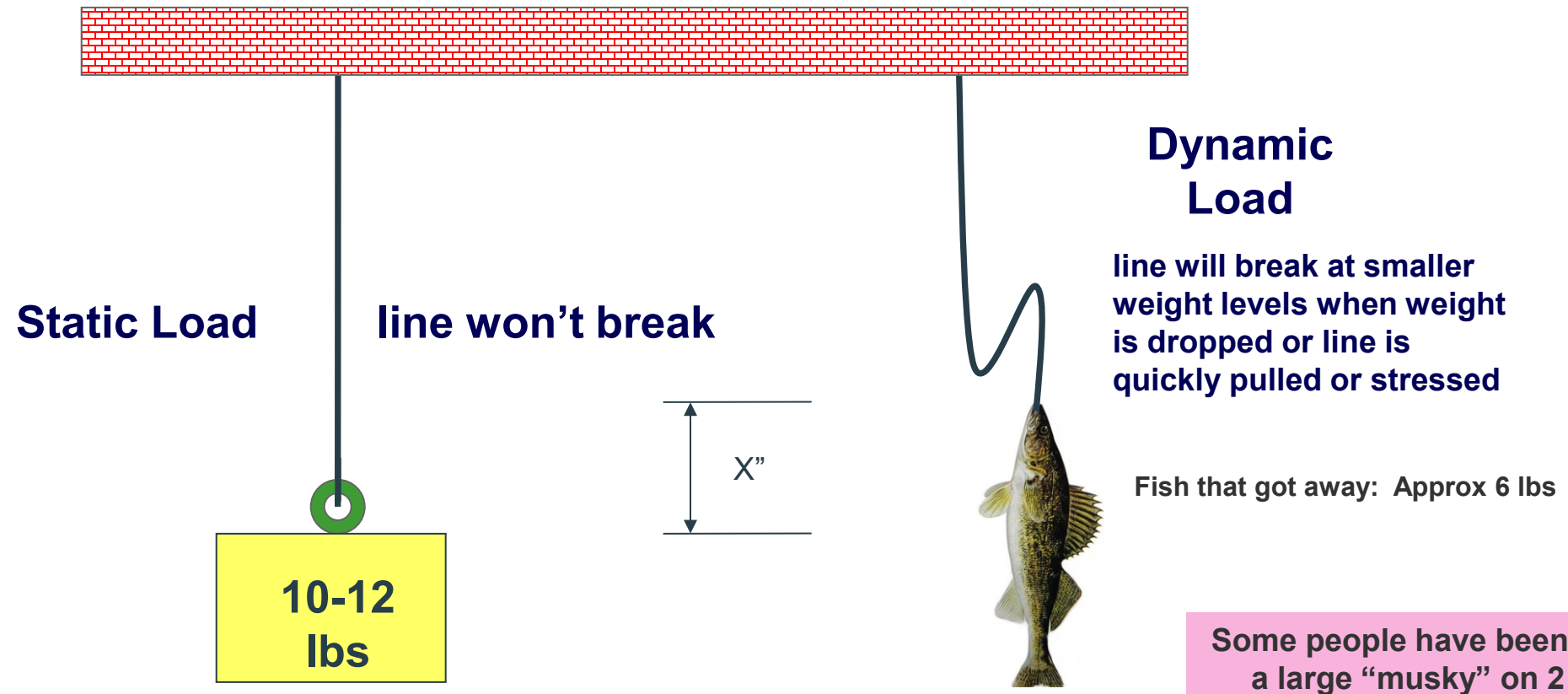
Short circuit forces are all acting in 3-D  
(combination of axial/radial/angular).

They can reach summative levels of up to 2+ million lbs,  
per phase, **INSTANTANEOUSLY!**

# Physics of Materials: Static vs Dynamic Stress

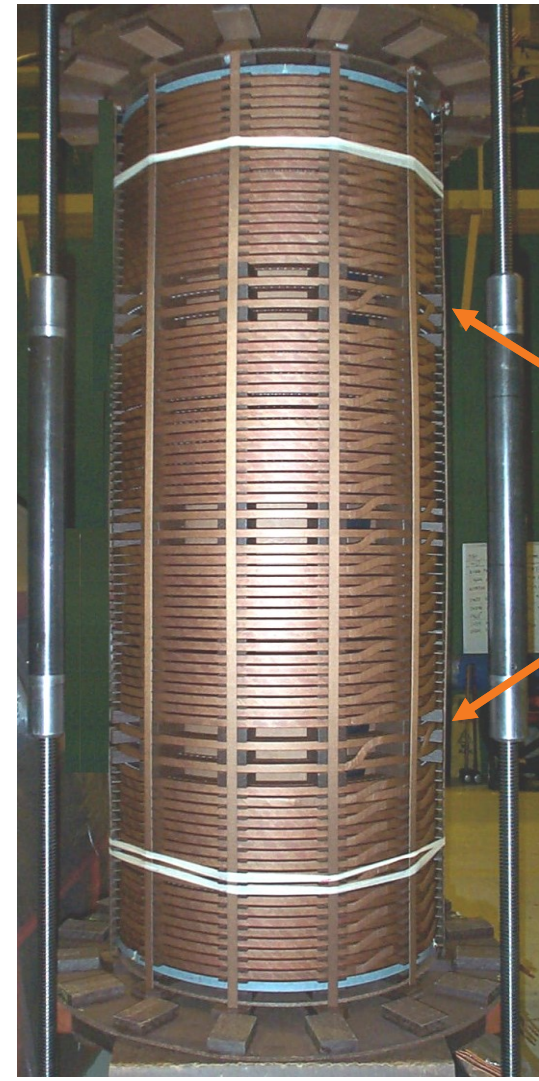
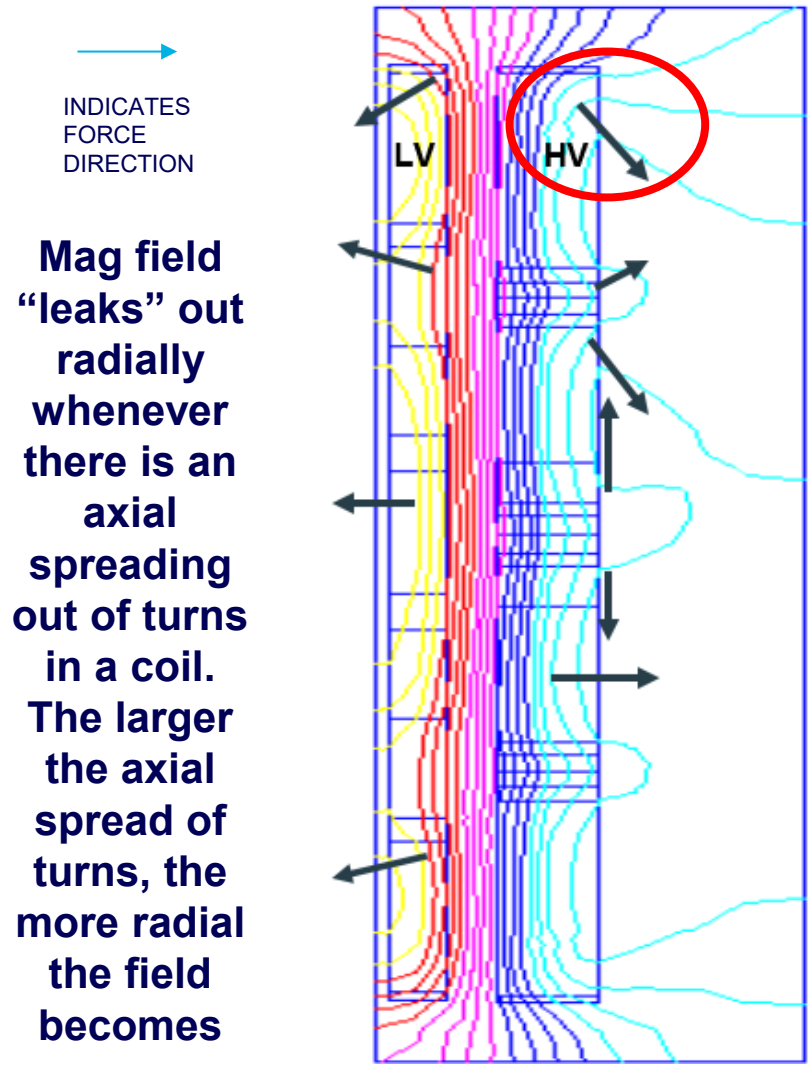
We know that: All materials behave differently under static (stationary) versus dynamic (moving) load conditions

Example using a weight suspended from a 10 lb test fishing line





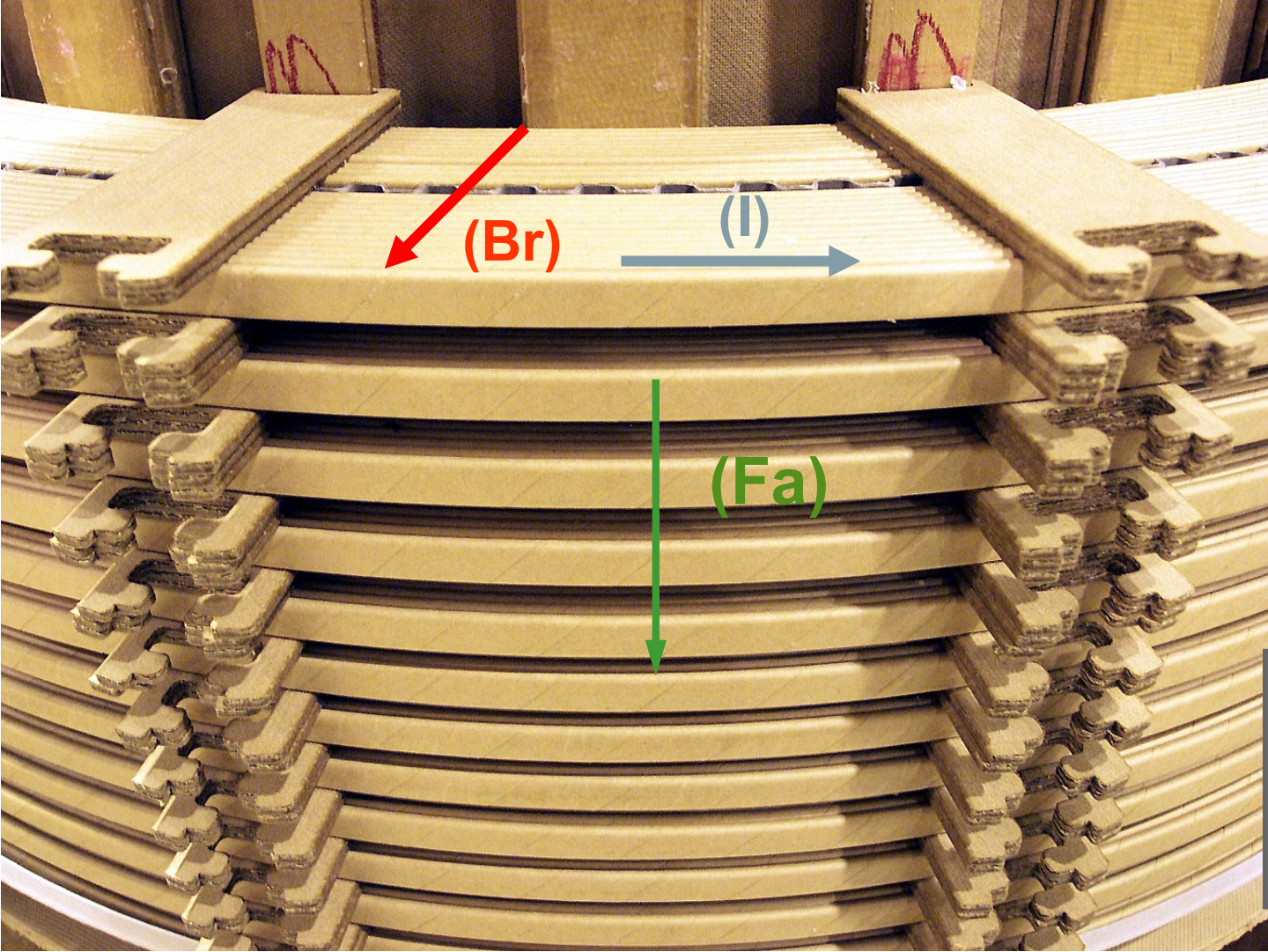
# Visualization of Magnetic Fields and Forces



Axial locations of where HV DETC taps are located

Finite Element Analysis of Leakage Flux Between Coils

# Axial Forces - (Applying Left Hand Rule)



Current (I)

Flux (B)

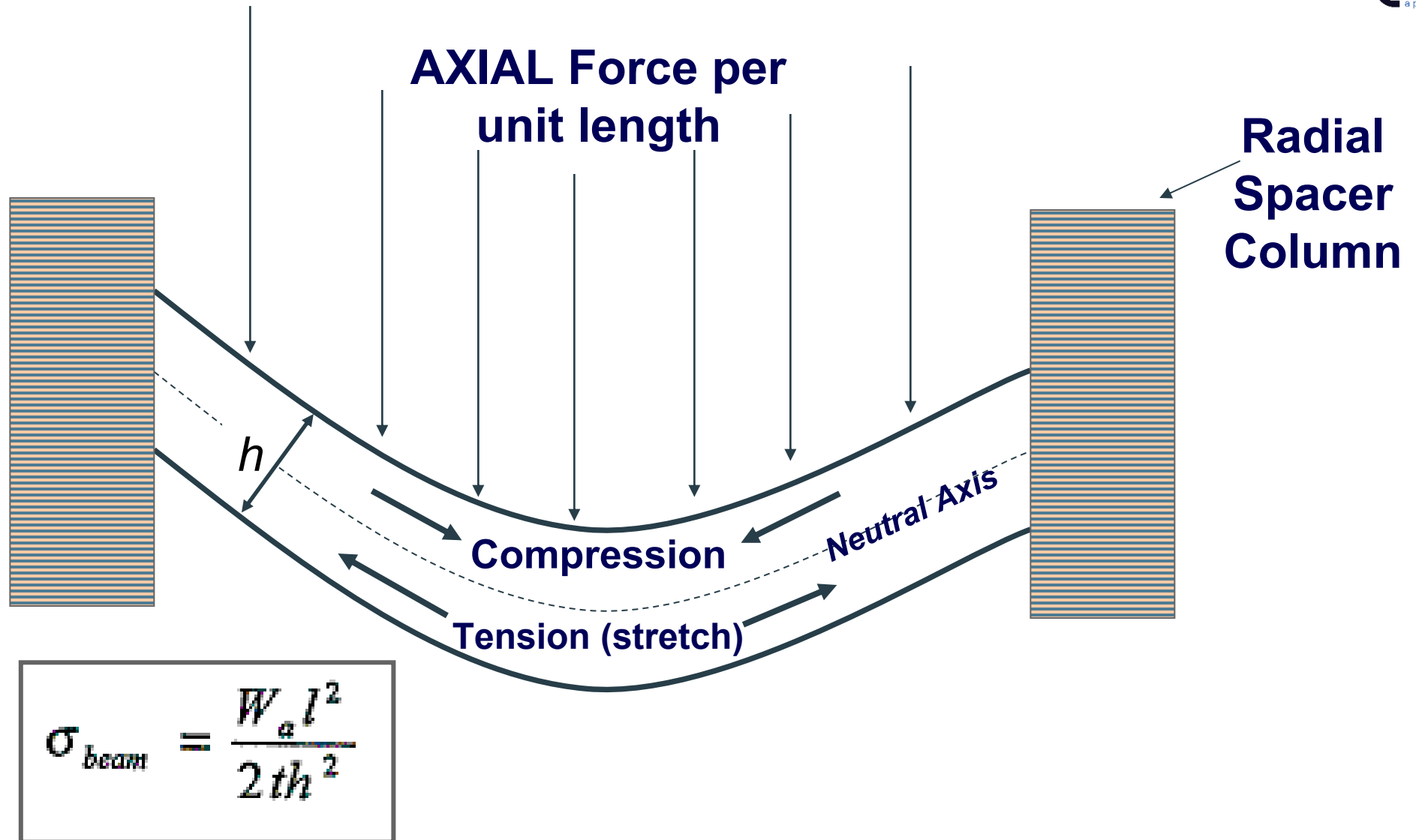
Force (F)

Length of beam:

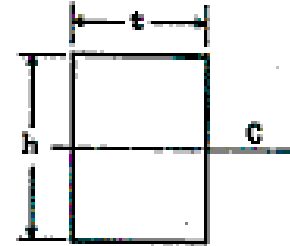
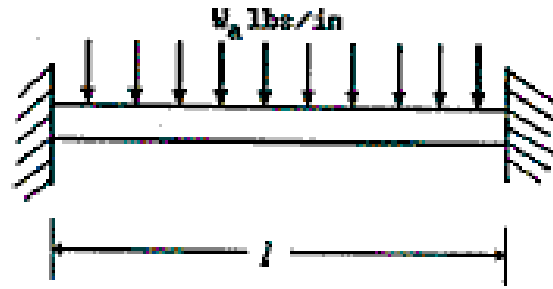
$$l = \frac{2 \pi R_{OD}}{m} - W_b$$



# Beam Bending Under Load (elevation view)



# Beam Bending Stress



$$\sigma_{beam} = \frac{W_a l^2}{2th^2}$$

where:

- $R_{OD}$  = Winding O.D. (inches)
- $W_{ks}$  = Keyspacer Width (inches)
- $m$  = Number of Key Spacer Strings
- $F_{max}$  = Maximum Force on a Disk or Conductor (lbs)

**Length of beam:**

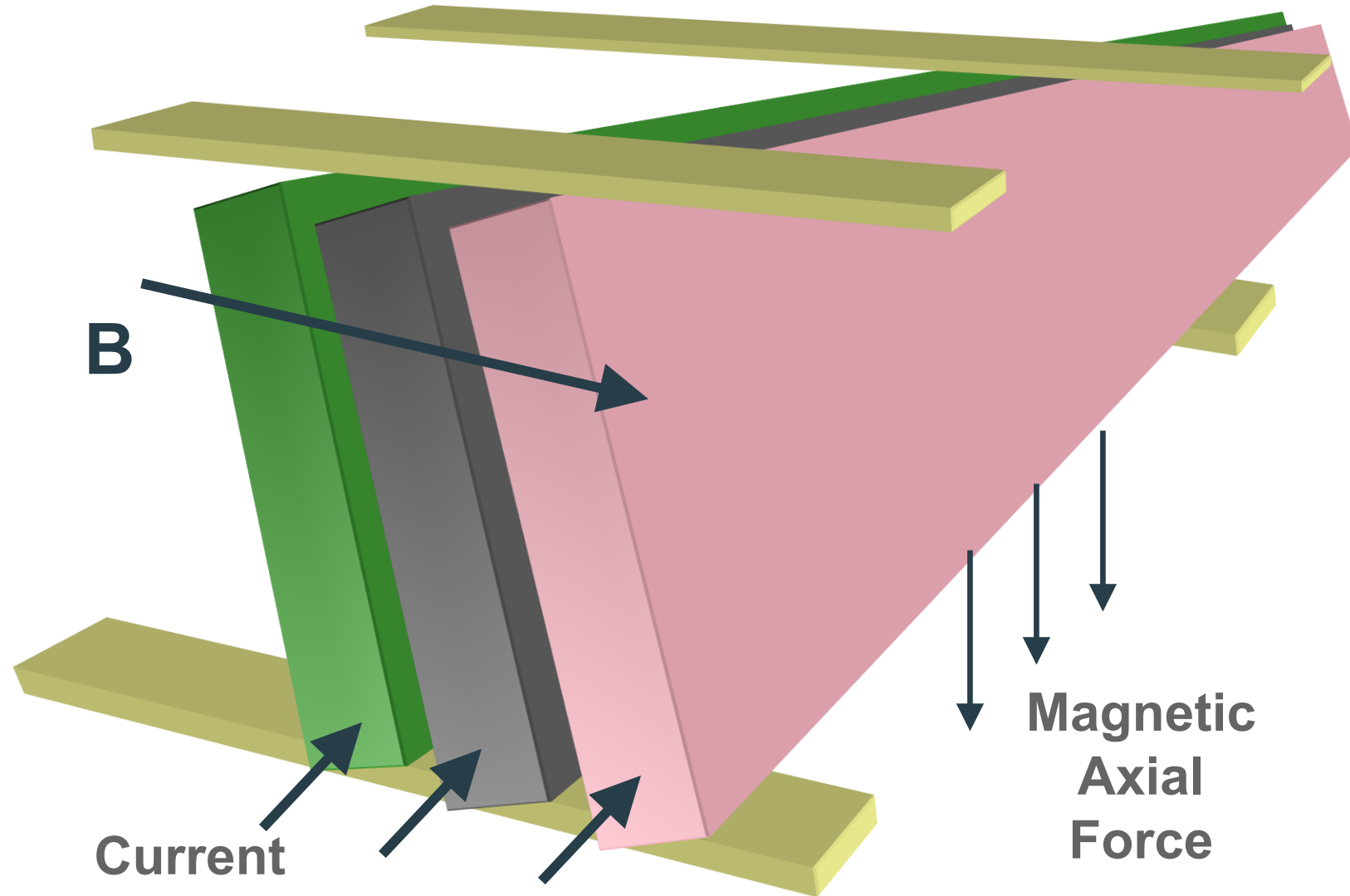
$$l = \frac{2\pi R_{OD}}{m} - W_{ks}$$

**Linear Load:**

$$W_a = \frac{F_{max}}{l}$$

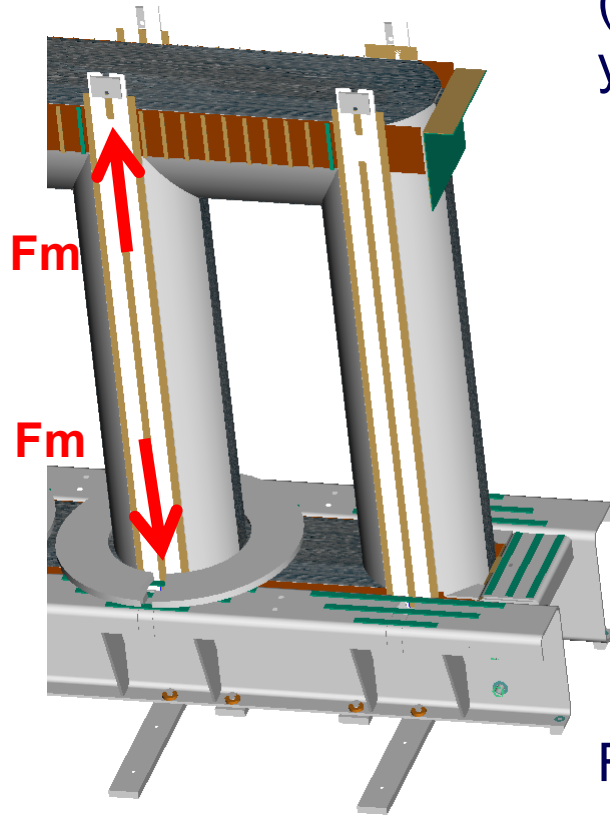


# Conductor Tipping/Tilting



# Stress in Tie Bars (Verticals)

The minimum cross-sectional area of the tie bar ( $A_{tb}$ ) is determined by the force applied and the yield point of the tie bar material.



Yield Strength of Tie Bar = 100,000 PSI

70% of yield = 70,000 PSI

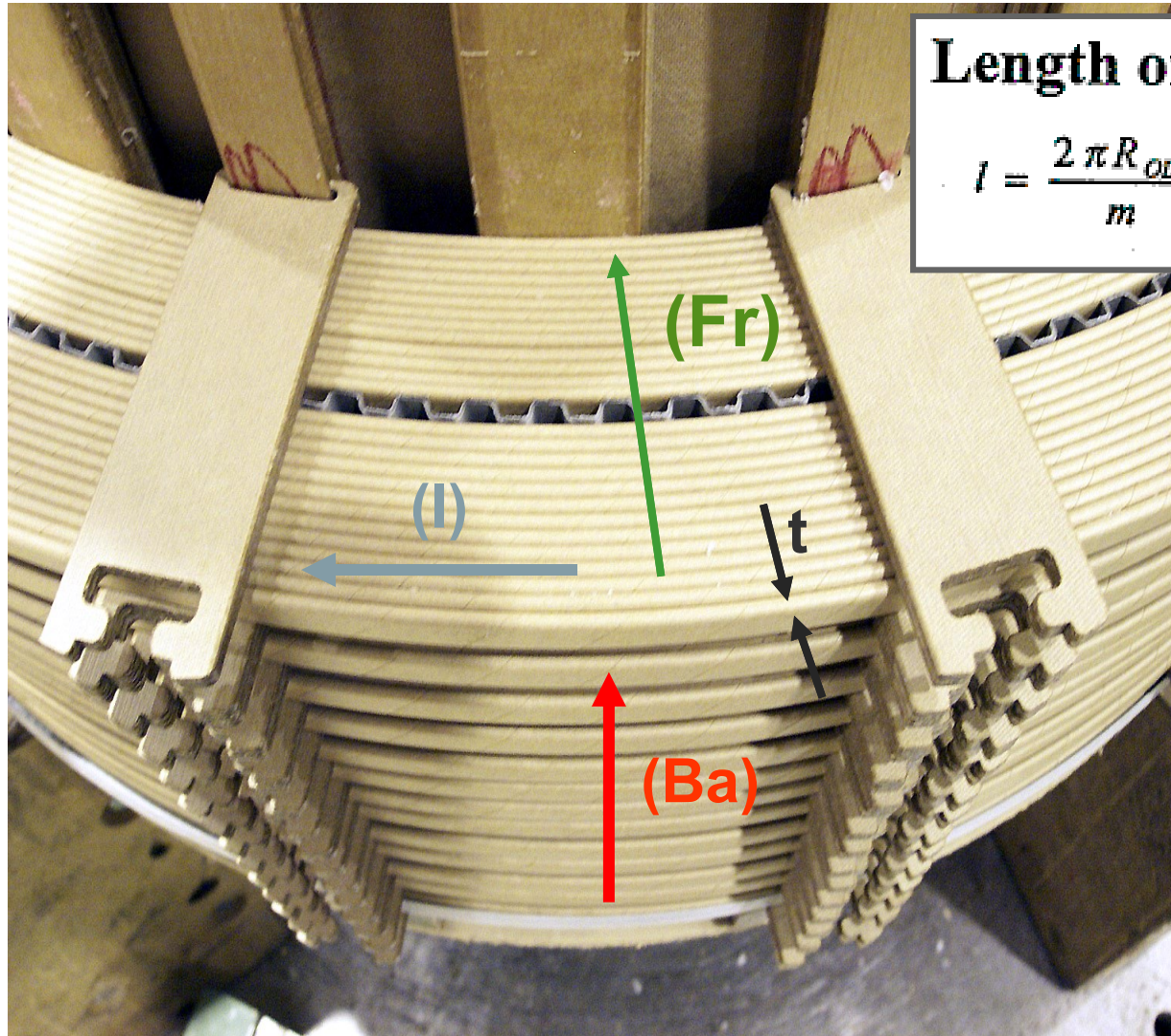
$F_m/2$  to get minimum area per tie bar (2 per phase)

$$A_{tb} = \frac{F_m/2}{70,000}$$

$F_m$  is the larger of:

- maximum axial short circuit force (PSI)
- maximum winding sizing per phase (PSI)

# (Inward) Radial Forces – Buckling (inner coil)



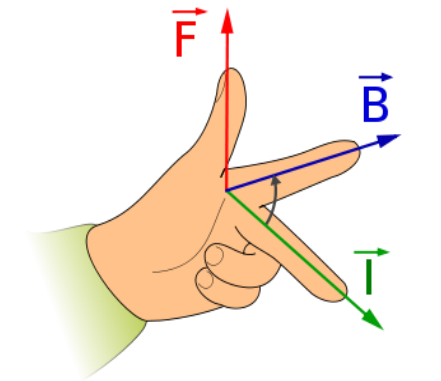
**Length of beam:**

$$l = \frac{2 \pi R_{OD}}{m} - W_{kr}$$

Current (I)

Flux (B)

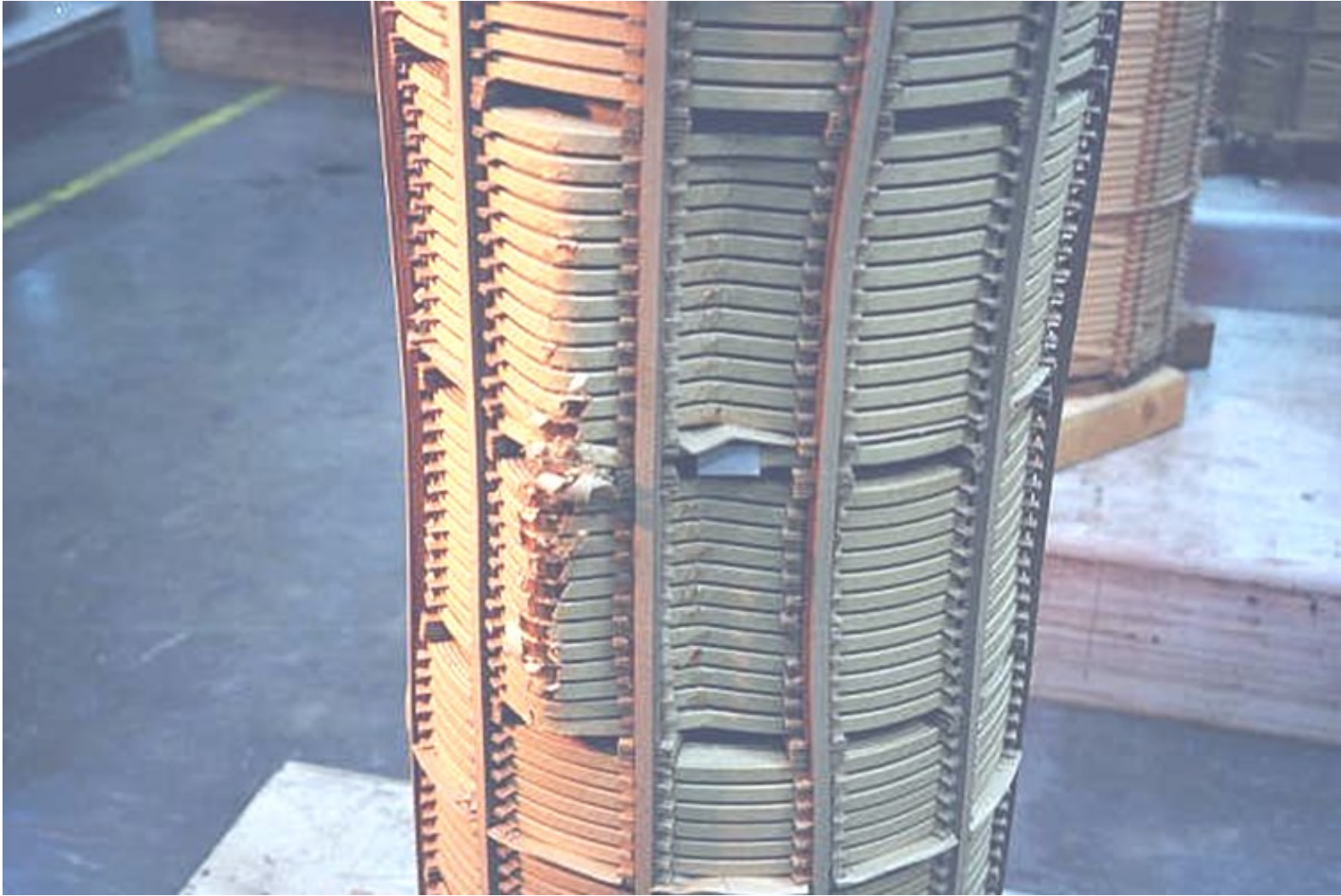
Force (F)



Left-Hand Rule

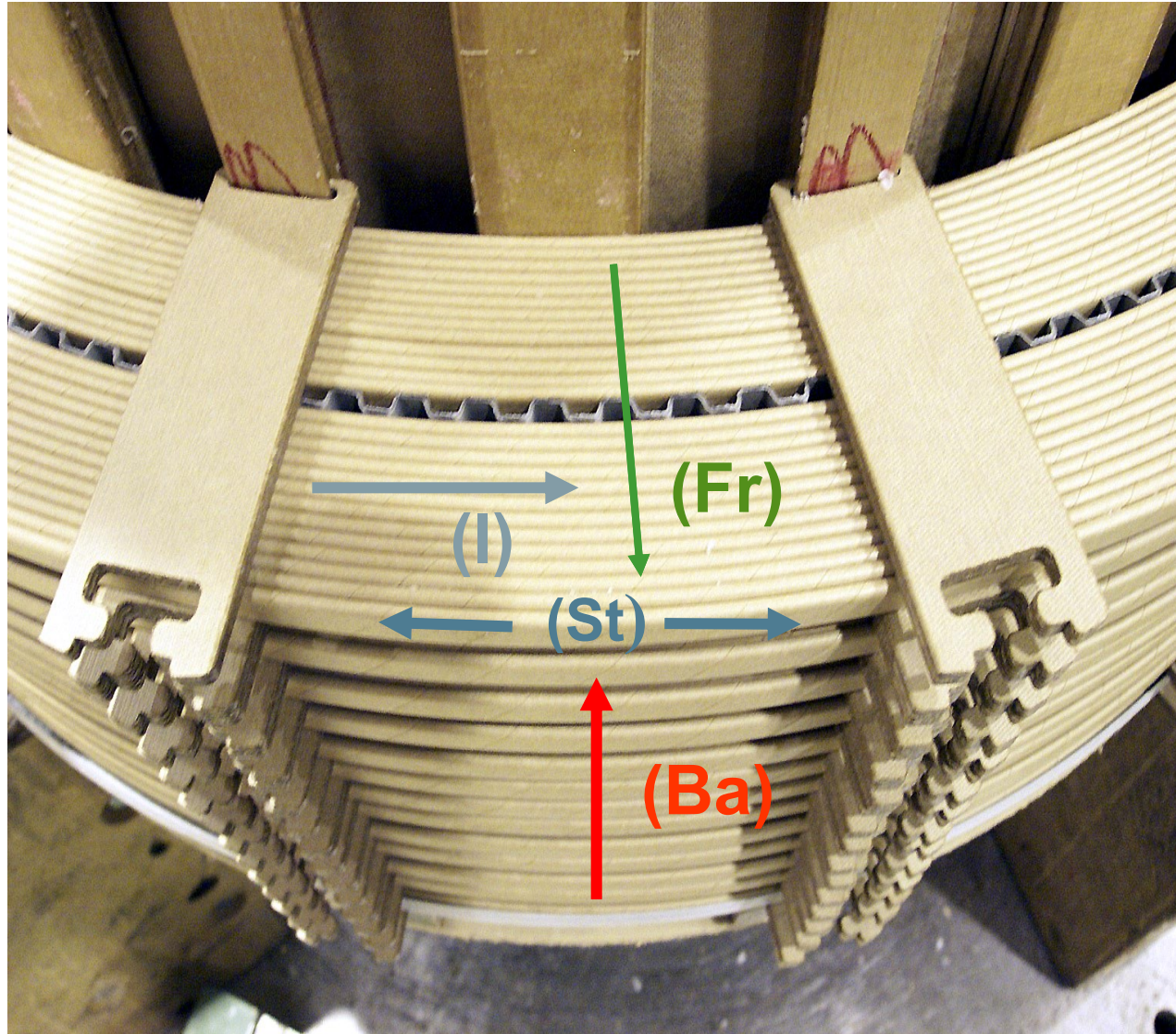


# Buckling Photo - Inner Winding Forced Into Failure in a Laboratory Setting...





# OUTWARD Radial Forces – Hoop Stress (outer coil)

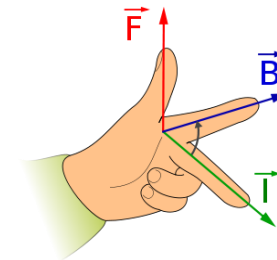


Current ( $I$ )

Flux ( $B$ )

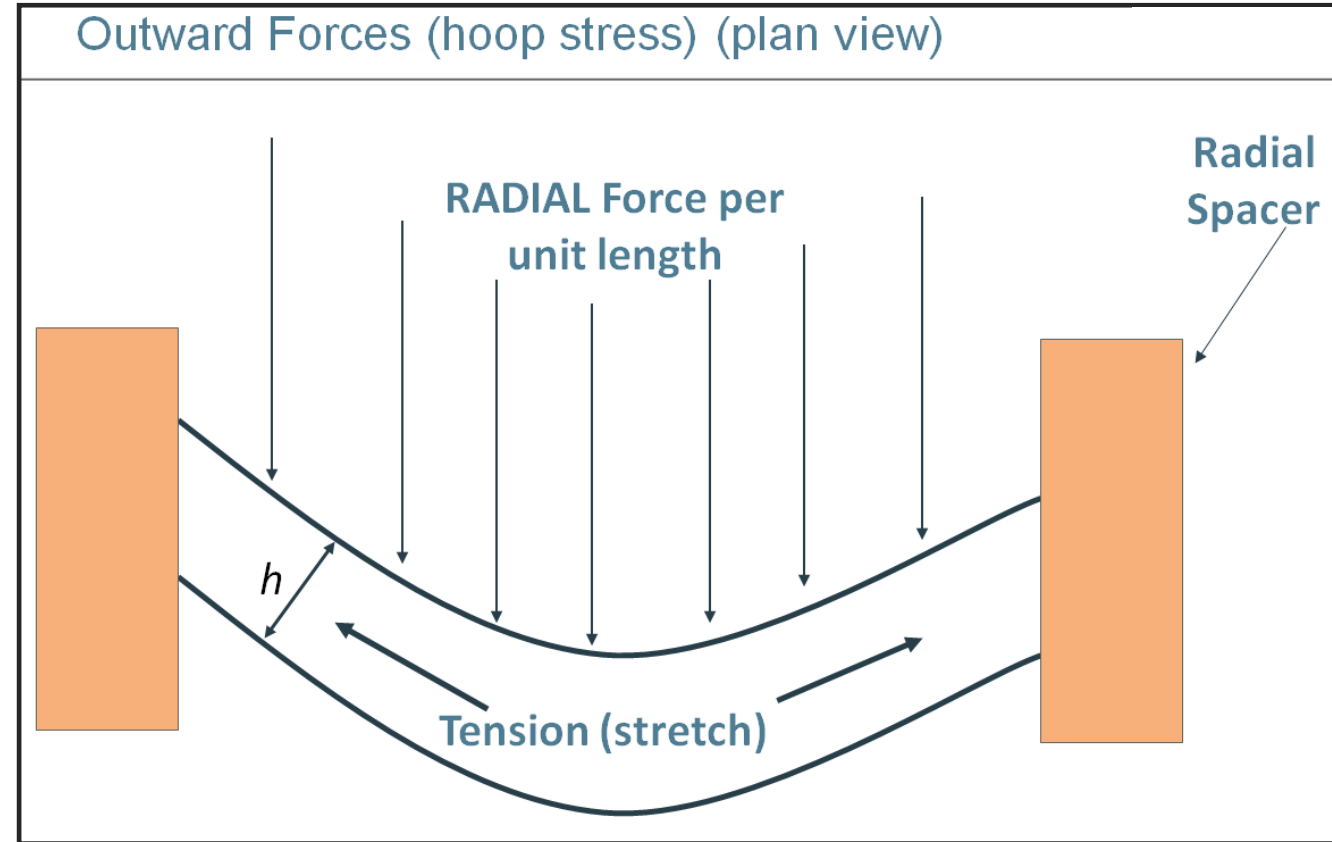
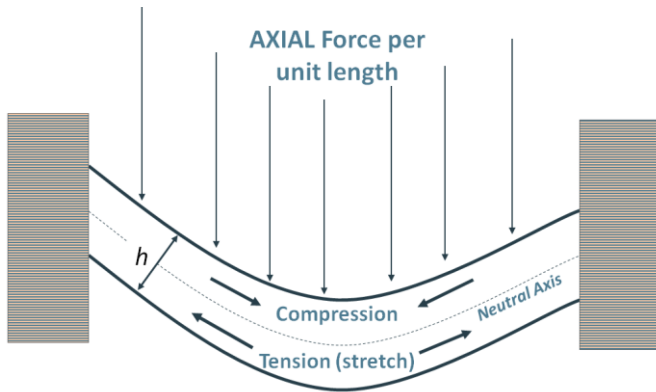
Force ( $F$ )

Tensile  
Stress ( $St$ )



Left-Hand Rule

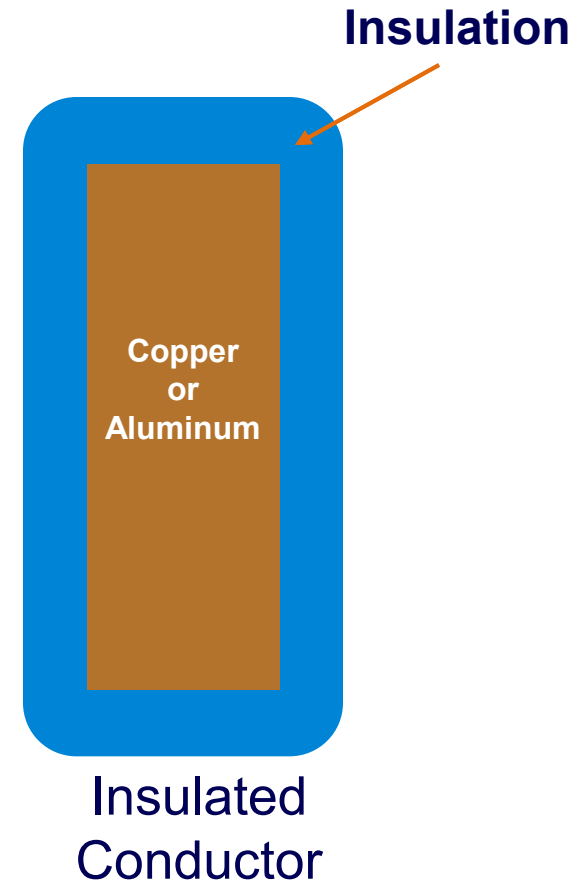
# Outward Forces (hoop stress) - Outward Radial Force exerts Tensile Stress only



**No neutral axis**

# Winding Temperature During a Short Circuit

- Calculated on basis that all heat is stored (heats up too quickly to radiate heat to equilibrium)
- Temperature not to exceed
  - 250°C for copper
  - 200°C for EC grade aluminum
- Method defined on IEEE C57.12.00-2000 section 7.4.



# Winding Temperature During a Short Circuit

Approximate method:

$$T_f = \frac{(S_{\Delta k})^2 t}{K_m} + T_{OR} + T_a$$

$T_f$  = final winding temperature at end of a short circuit (°C)

$T_{OR}$  = maximum top liquid temperature rise over ambient temperature (°C)

$T_a$  = ambient temperature (°C)

$S_{\Delta k}$  = winding current density at symmetrical short circuit current (W/dm<sup>2</sup>)

$t$  = short circuit duration (s).

$K_m$  = 156 for copper / 73 for EC grade aluminum





## Part 5 – Calculation Example:

- Calculate short circuit current and asymmetrical offset factor

# Back to our formulas again....

**ASYM: MECHANICAL DAMAGE**

$\phi = \text{Arc Tan } \frac{\omega L}{R}$

**4 SYMMETRICAL**

$K = \frac{I_{\text{Asy (peak)}}}{I_{\text{Sym (RMS)}}$

**1 RATED AMPS**

$\tau = \frac{L}{R}$   
Resistance is essentially a dampening factor

**TO FIND ANY POINT IN THE TIMELINE**

**4 SYMMETRICAL**

**2 3**

**ASYMMETRICAL (PEAK) current**

$I_{SC}(\text{peak asym}) = K I_{SC}$  where

$K = \left\{ 1 + \epsilon \left[ \frac{1 - \cos(\phi + \frac{\pi}{2} - \omega t)}{\sin \phi} \right] \sqrt{2} \right\}$  per unit

OFFSET VALUE MAINLY AFFECTED BY  $X/R$   
 $\phi = \arctan \frac{X}{R}$ , radians

FAULT TIME IN RADIANS WORSE CASE AT  $V=0$

$Z_S = \frac{MVA_{\text{TRANS}}}{MVA_{\text{SC}}}$

$\tau = X/R$

$\frac{1}{\tau} = R/X$

**THIS FORMULA TAKES YOU RIGHT TO FIRST ASYMMETRICAL PEAK! POINT A**

# Example of How to Calculate SC Current

Assume we have a transformer with a 69kV primary and the following known data:

Transformer MVA = 30 MVA base

Rated amps on LV (@ 30 MVA) = 1000 amps

Tested load loss @ 30 MVA: 72.0 kw

Tested impedance @ 30 MVA: 8.0% (= 0.8 p.u.)

To find  $I_{sc}$ (RMS symmetrical) and  $I_{sc}$ (Peak Asym), we must perform 3 steps in the following order:

1. Determine  $I_{sc}$  (RMS symmetrical)
2. Determine offset (asymmetrical) “K” factor
3. Apply derived data from 1. and 2. to determine peak offset asymmetrical amps.

Next 

# Example of How to Calculate SC Current

## STEP 1: Find $I_{SC}$ (RMS symmetrical)

Note:  $Z_T$  and  $Z_s$  are in p.u.

$$I_{SC} = \frac{I_R}{Z_T + Z_S}$$

$$I_{SC} = \frac{1000}{0.08 + 0} = 12,500A$$

OR, using the other formula ...

$$I_{SC} = \frac{100}{8\%+0\%} \times I_{\text{rated}}$$

$$I_{SC} = \frac{100}{8\%+0\%} \times 1000A = 12,500A$$

Symmetrical Current without  $Z_s$

Symmetrical Current with  $Z_s$

$$I_{SC} = \frac{I_R}{Z_T + Z_S}$$

$$I_{SC} = \frac{1000}{0.08 + Z_s}$$

$$Z_s = \frac{MVA_T}{MVA_S} = \frac{30}{9800} = 0.31\%$$

$$I_{SC} = \frac{1000}{0.08 + 0.0031} = 12,034 A$$

Note:  $Z_s$  is derived from C57.12.00-2010 Table 15 if not specified from customer.

Difference (with vs without  $Z_s$ ) is almost 500A or 4%

Next 



# Example of How to Calculate SC Current

## Step 2: Determine the “K” factor:

To find “K” factor, we need to determine %R and X/R ratio...

$$K = \left\{ 1 + \left[ e^{-\left(\phi + \frac{\pi}{2}\right)\frac{r}{x}} \right] \sin \phi \right\} \sqrt{2}$$

### 1. Find %R

$$\%R = 100x \frac{\text{Load Loss (kW)}}{KVA_T} = \frac{100x72}{30,000} = 0.24\%$$

### 2. Find X/R

$$\frac{X}{R} = \frac{Z_T}{\%R} = \frac{8\%}{0.24\%} = 33.33$$

Plug these values into next equation

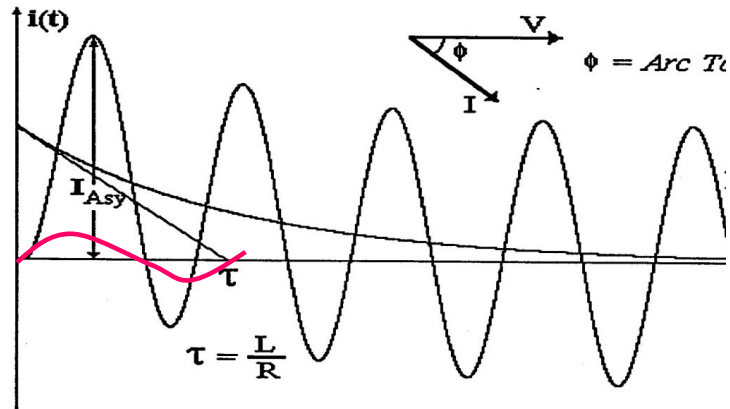
# Example of How to Calculate SC Current

Step 2 (continued): Determine the “K” factor:

$$K = \left\{ 1 + \left[ e^{-\left(\phi + \frac{\pi}{2}\right) \frac{r}{x}} \right] \sin \phi \right\} \sqrt{2}$$

$$K = \left\{ 1 + \left[ e^{-\left(\tan^{-1}(33.33) + \frac{\pi}{2}\right) * \frac{1}{33.33}} \right] * \sin(\tan^{-1}(33.33)) \right\} * \sqrt{2}$$

$$K = 2.702$$



C57.12.00-2010 Table 14

$x/r$	$K$
1000.00	2.824
500.00	2.820
333.00	2.815
250.00	2.811
200.00	2.806
167.00	2.802
143.00	2.798
125.00	2.793
111.00	2.789
100.00	2.785
50.00	2.743
33.30	2.702

# Example of How to Calculate SC Current

## Step 3: Determine the $I_{sc}$ (Peak Asymmetrical):

Since  $I_{sc}(\text{peak asym}) = K \times I_{sc}(\text{RMS symmetrical})$

then ...

$$I_{sc}(\text{peak asym}) = 2.702 \times 12,500 \text{ amps} = \underline{33,750 \text{ amps}}$$

**FYI: Since  $F \propto I^2$**

**The Txf forces will see  $(33750 \text{ amps} / 1000 \text{ amps})^2 = (33.75)^2 = 1140 \times$  normal forces**

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a proleco company

# Questions