

# Regional Technical Seminar

## Short Circuit Design Considerations

Transformer Regional Technical Seminar

Minneapolis, MN

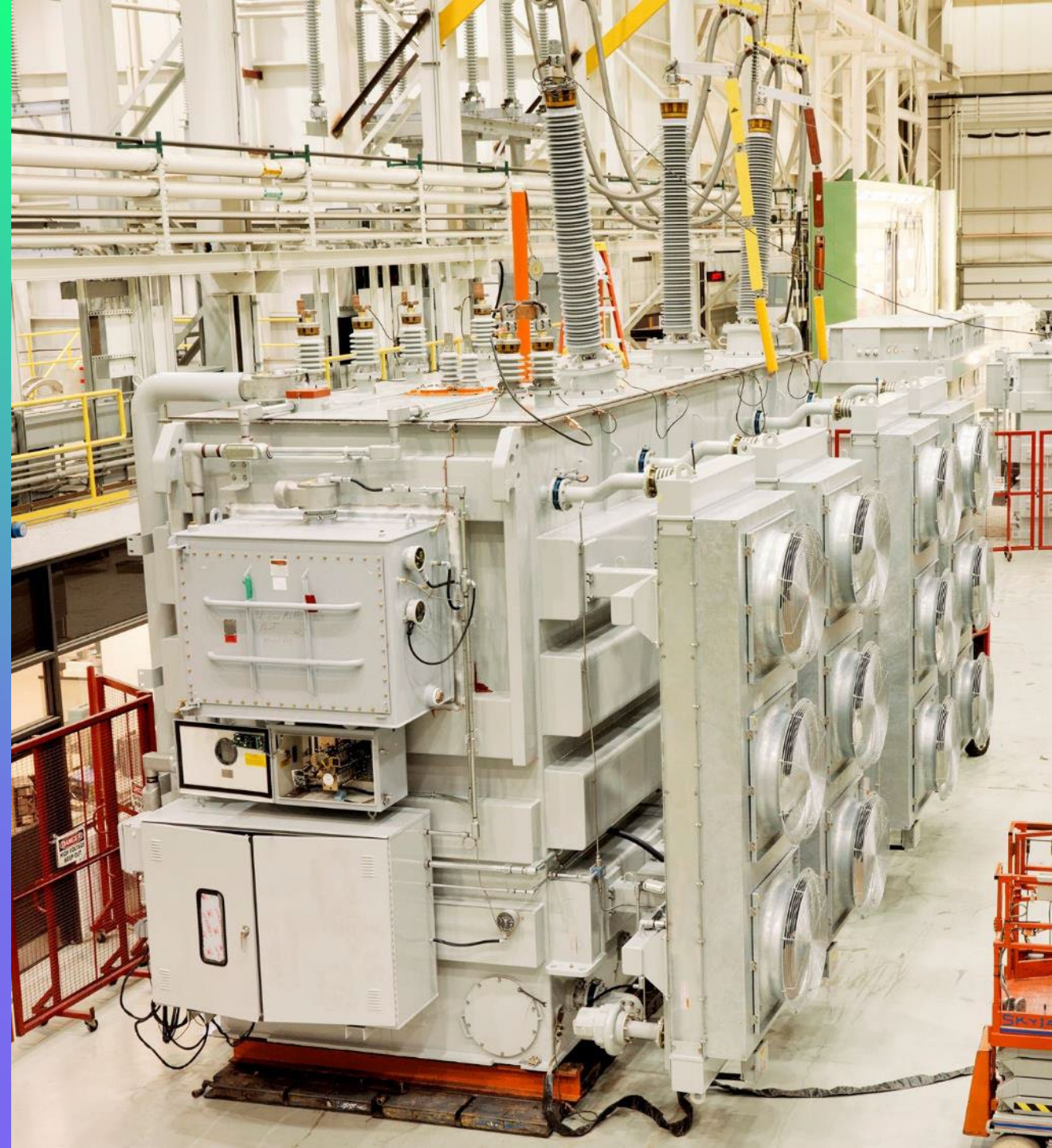
August 15, 2024

waukesha  
a prolec ge company

# Michael Liesch

Senior Electrical Design Engineer

*Mike started with Prolec GE Waukesha in 2016, bringing with him 3 years of experience in inspecting and testing transformers. He holds a Bachelors of Science degree in Electrical Engineering from the Milwaukee School of Engineering.*



# Agenda

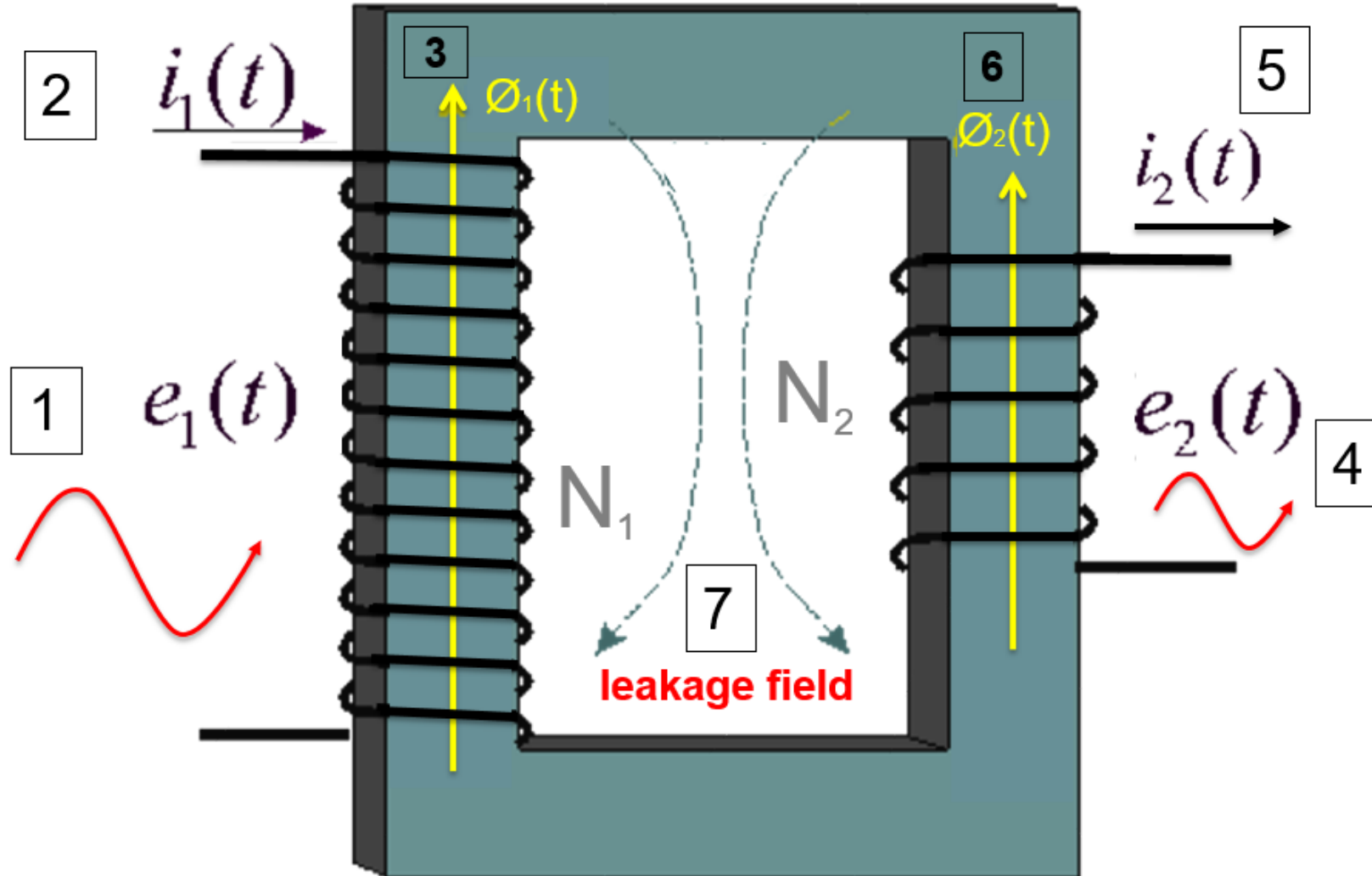
- Review transformers: How they work (textbook vs reality)
- Visualize relationship between Current and Magnetic Forces
- Understand fault current from time  $t = 0$  to  $t = ?$
- Understand formulas and variables to calculate short circuit currents
- Discuss fault types
- Calculation Example: Calculate short circuit amps
- Get a mental picture of magnetic forces acting within a transformer resulting from short circuit



## Part 1 – Transformer Basics:

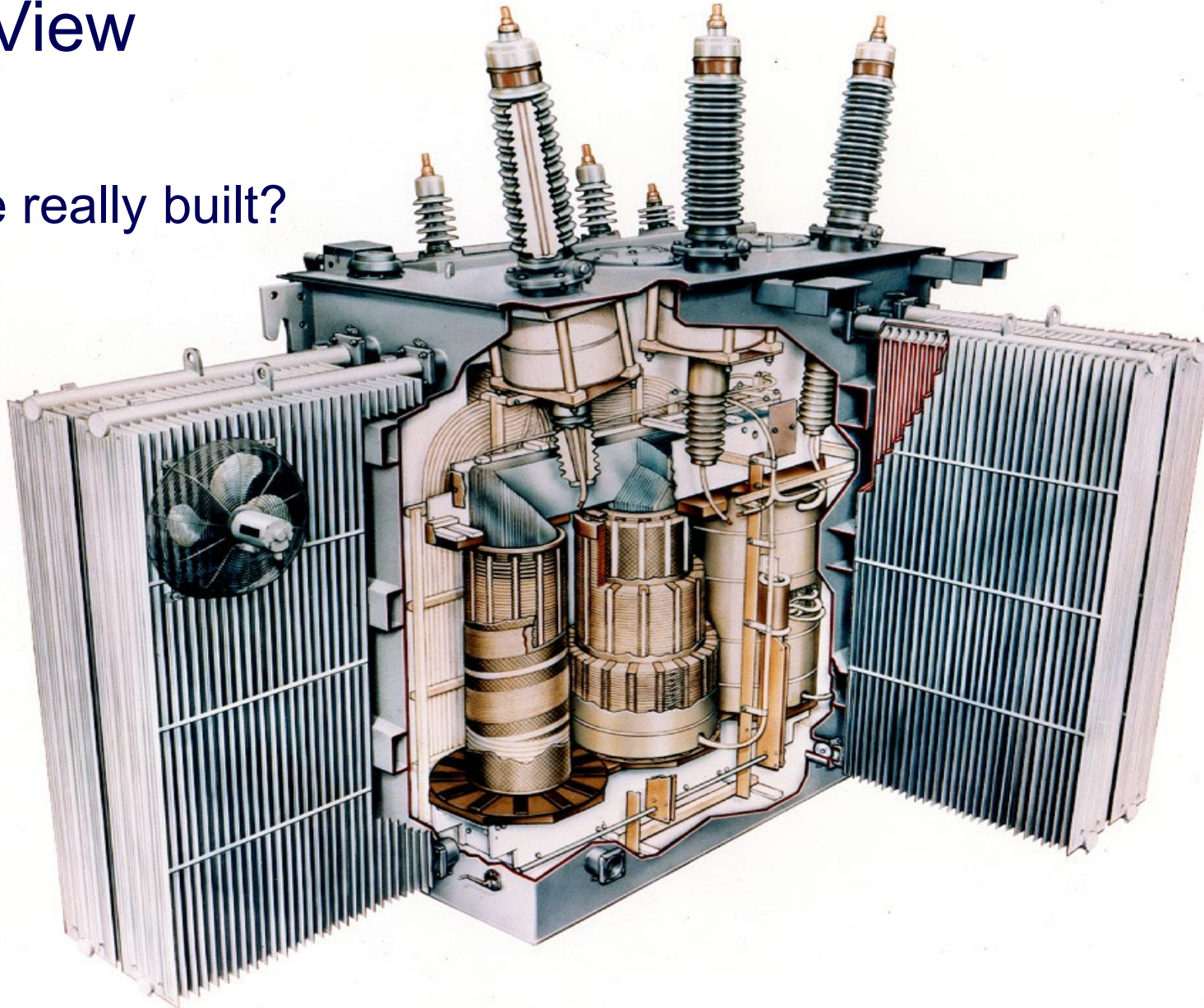
- How they work
- How they are actually built

# Textbook Transformer (step by step)

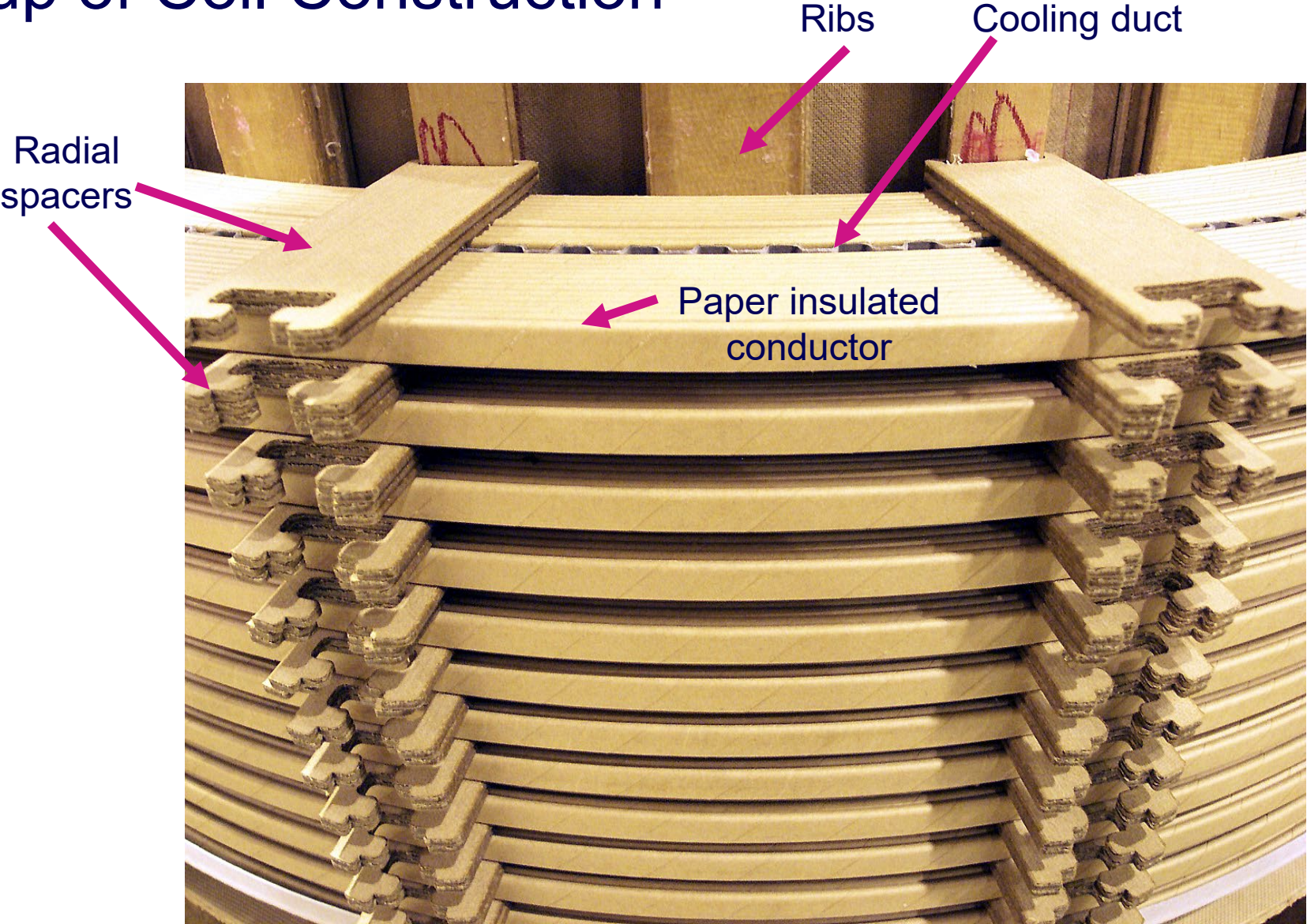


# Cutaway View

How they are really built?



# Close up of Coil Construction

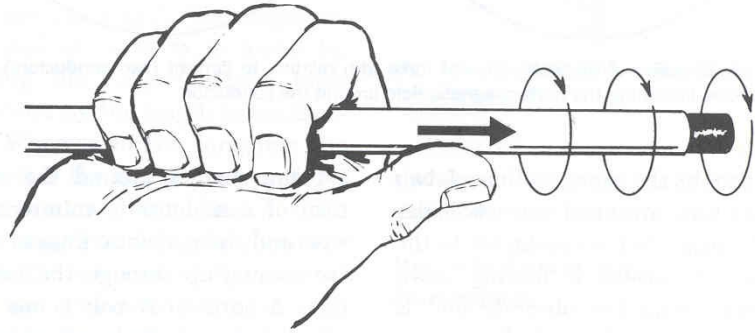


## Part 2 – Transformer Basics:

- Fundamentals of Magnetics and Forces
- Magnetic Fields Around Conductors
- Forces That Result



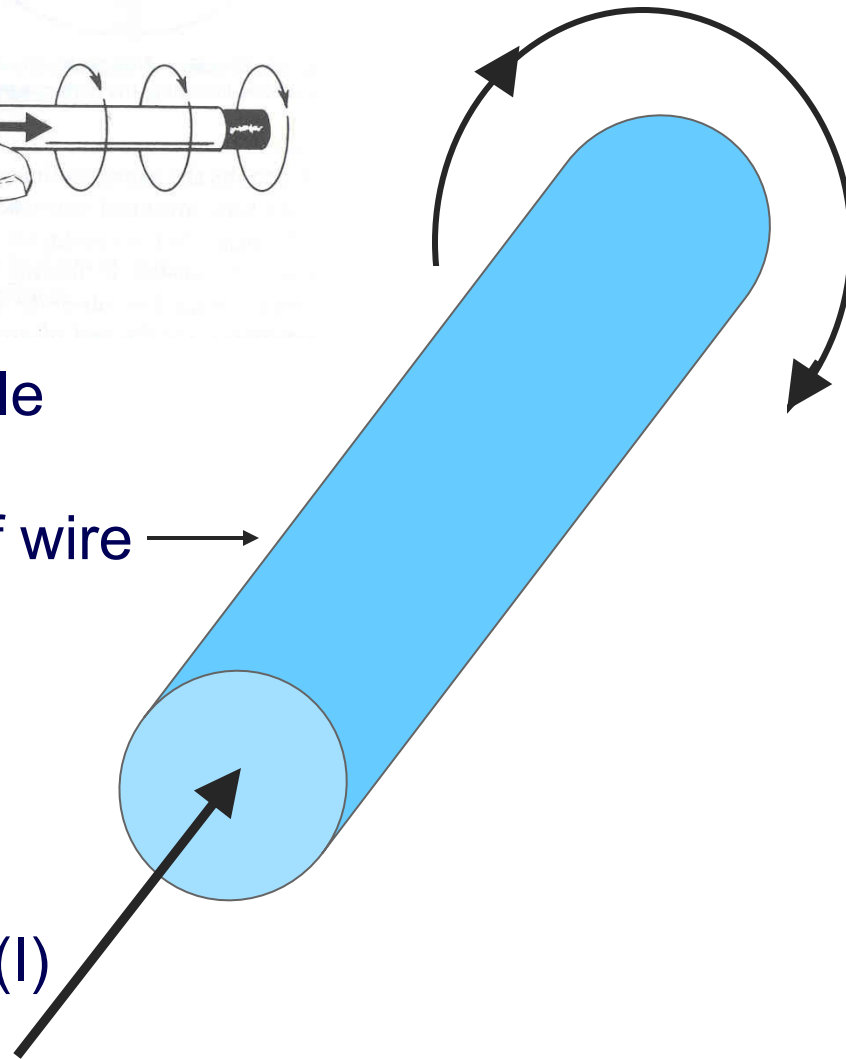
# Current & Magnetic Field Relationships



Right hand rule

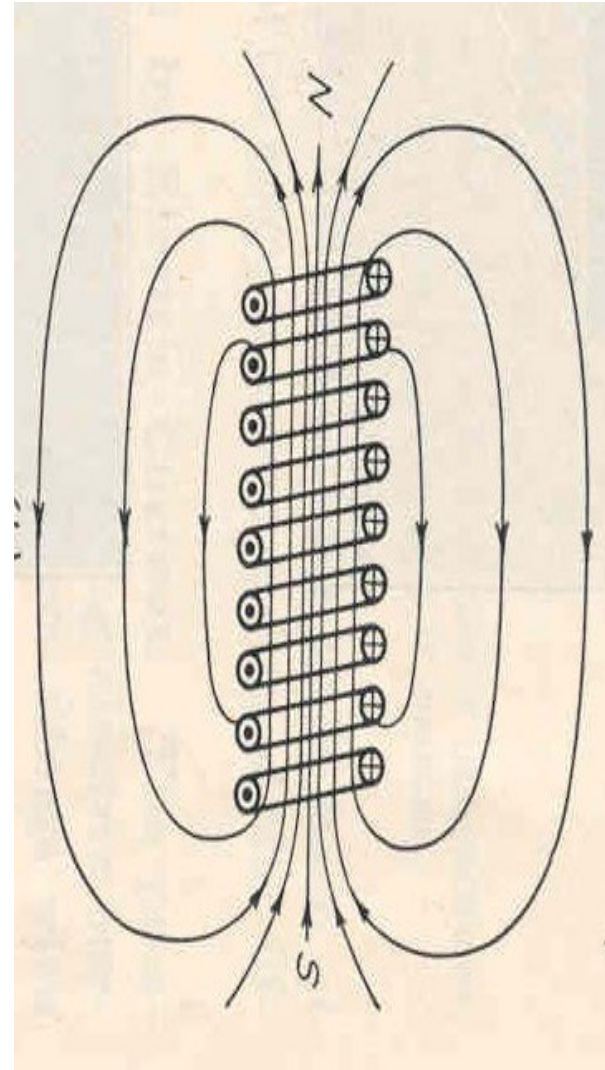
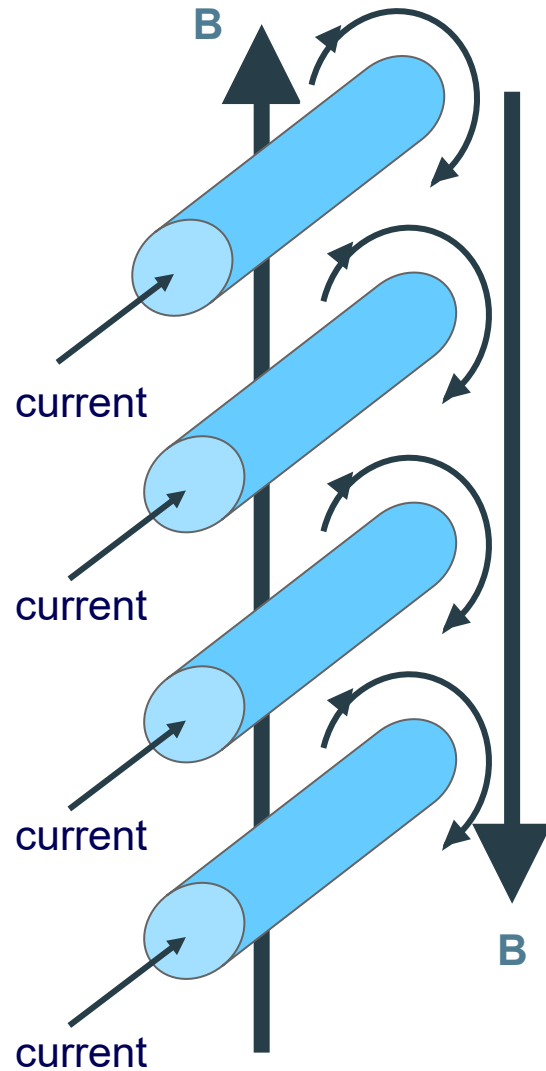
Consider a section of wire →

Current Flow (I) →



resulting  
magnetic  
field direction  
(CW)

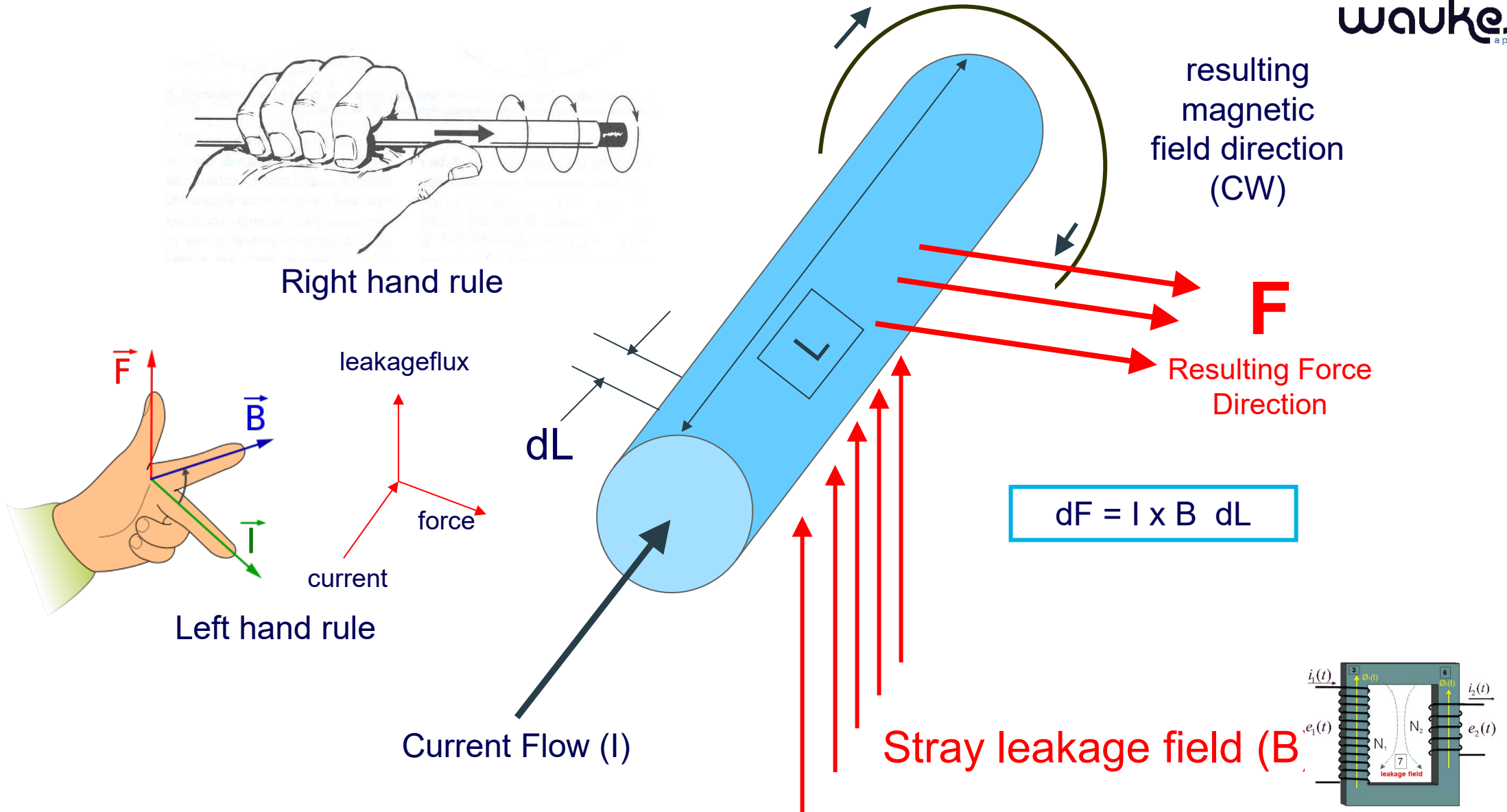
# Effect of Many Turns



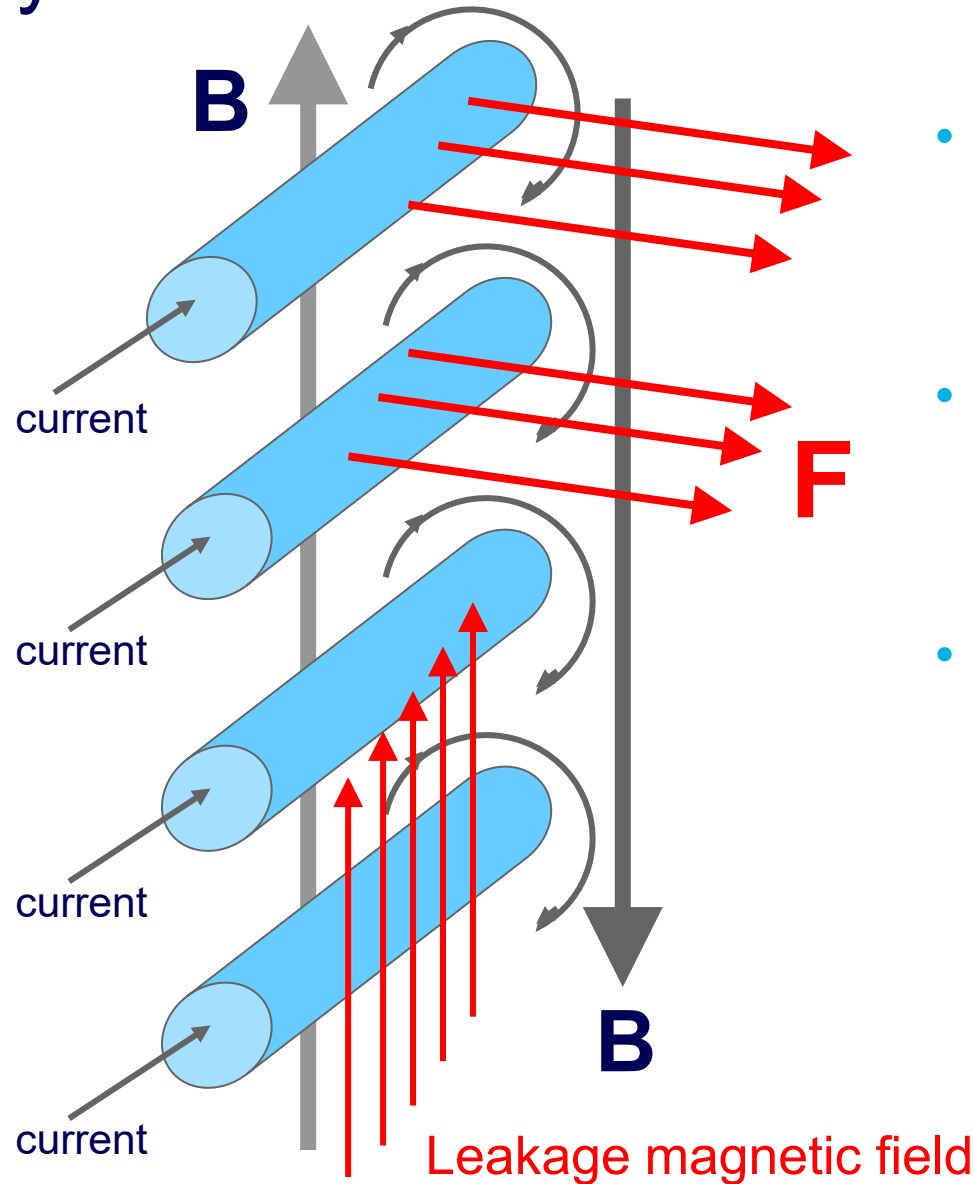
- Fields at inner/outer edges add together.
- One uniform magnetic path results
- Magnetic field (B) intensifies with # turns (N) or the current (I).

$$B \propto NI$$

# Leakage Field / Current / Force Relationships



# Effect of Many Turns



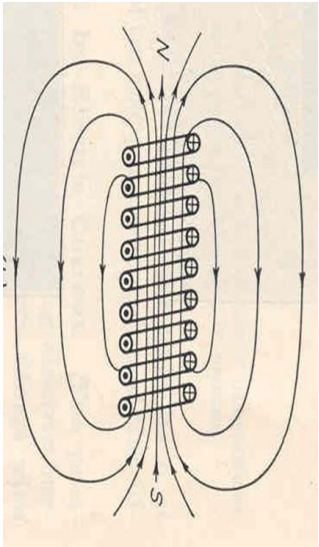
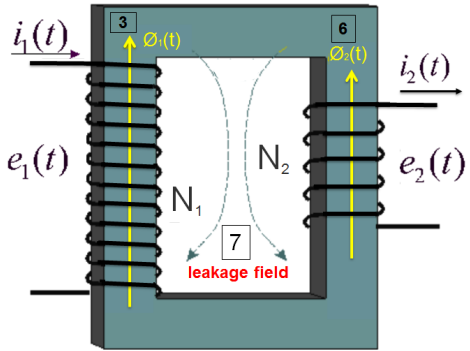
- Fields at inner/outer edges add together
- One uniform magnetic path results
- Magnetic Forces (F) intensifies with # turns (N)

$$B \propto NI$$

$$dF = N \times I B dL$$

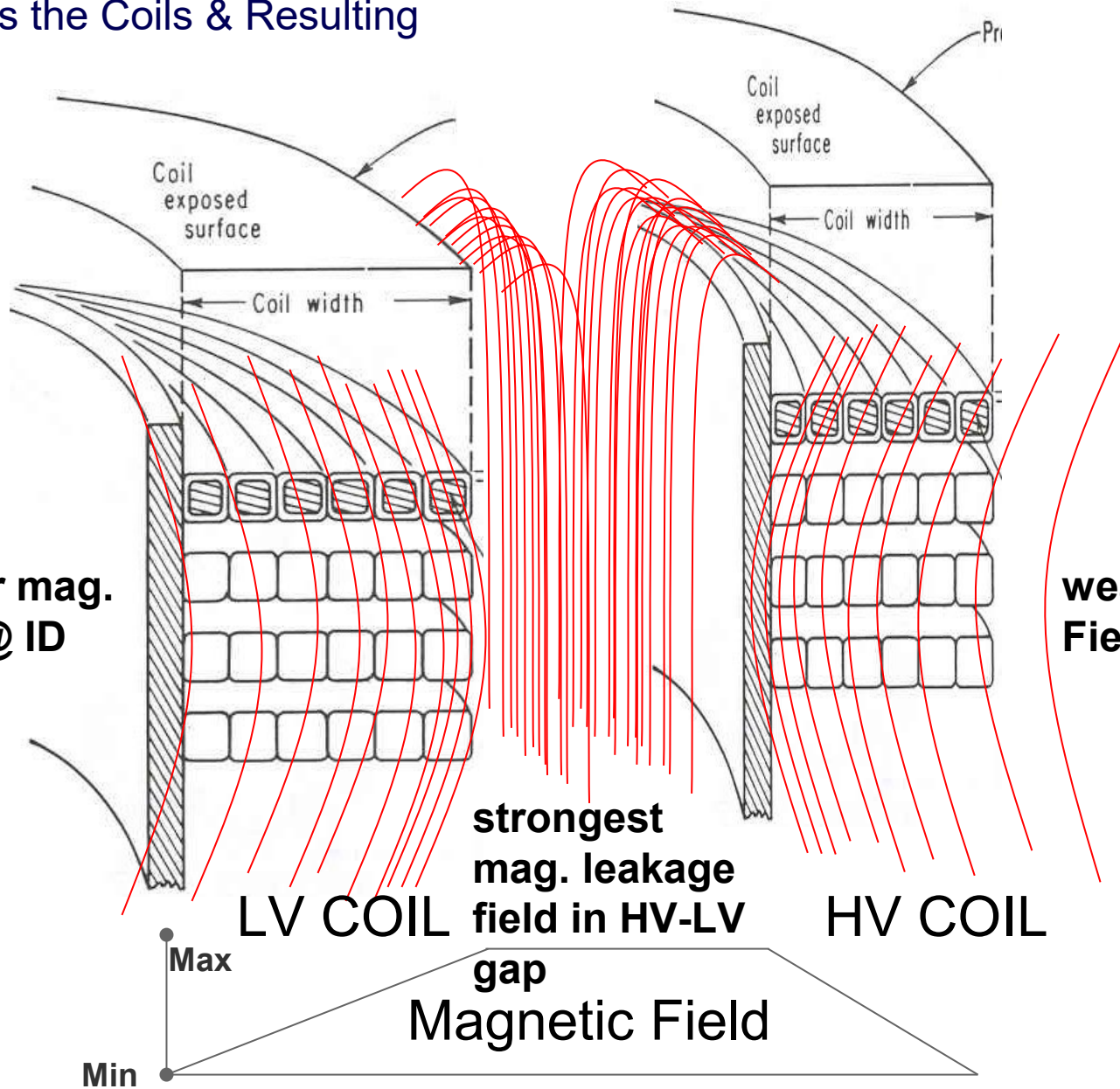
$$F \propto (NI)^2$$

# Magnetic "Leakage" Field Across the Coils & Resulting Forces



**weaker mag. Field @ ID**

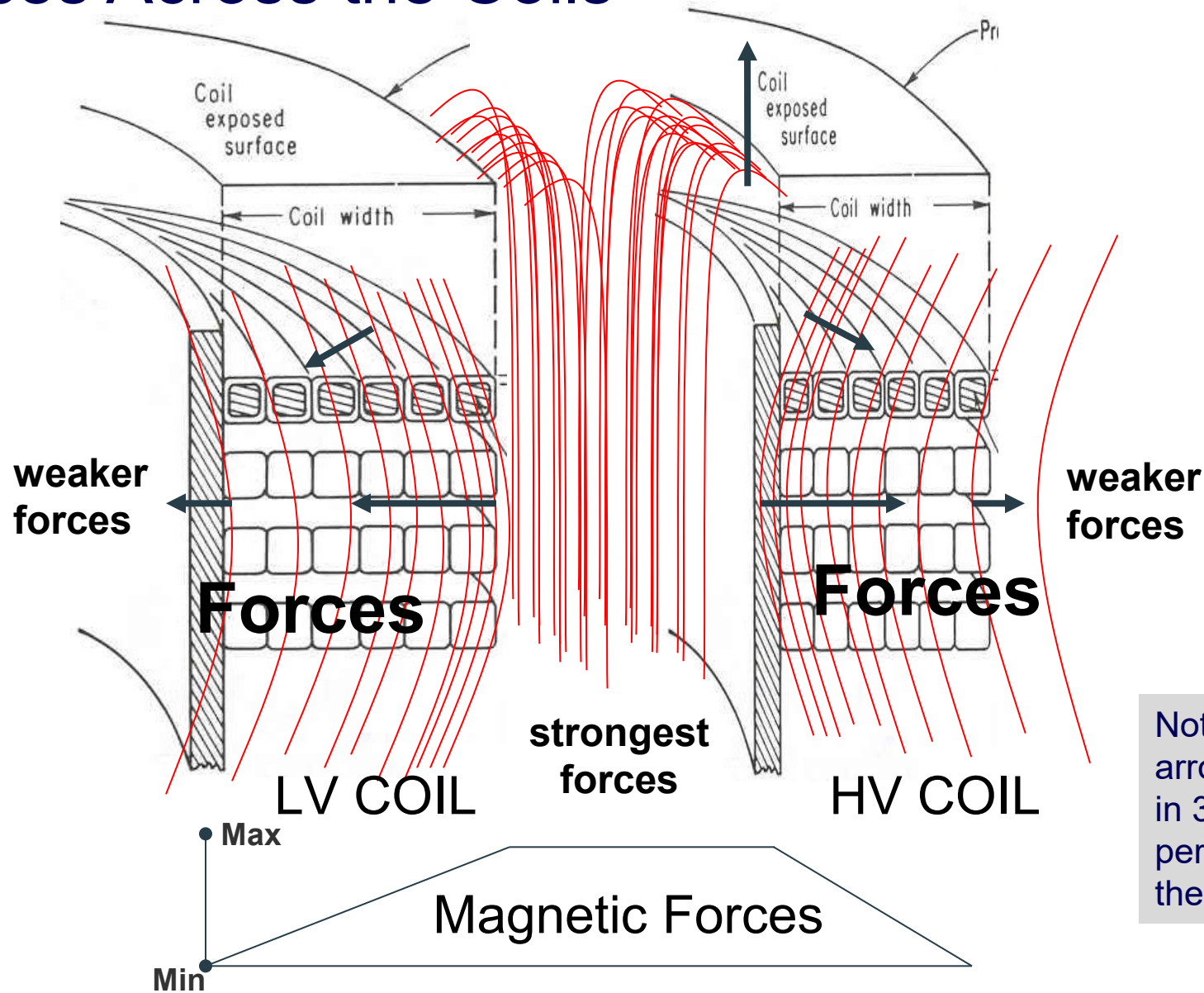
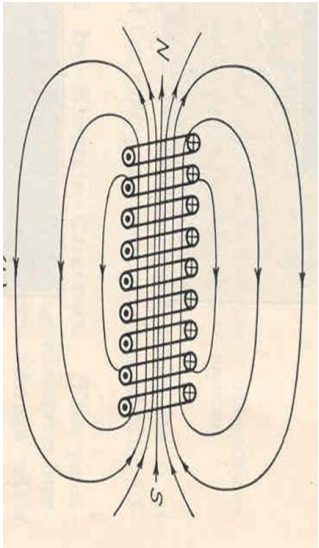
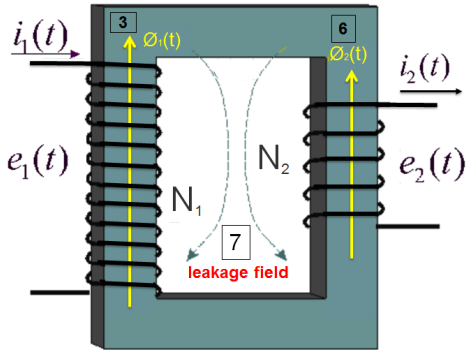
**weaker mag. Field @ OD**



**strongest mag. leakage field in HV-LV gap**

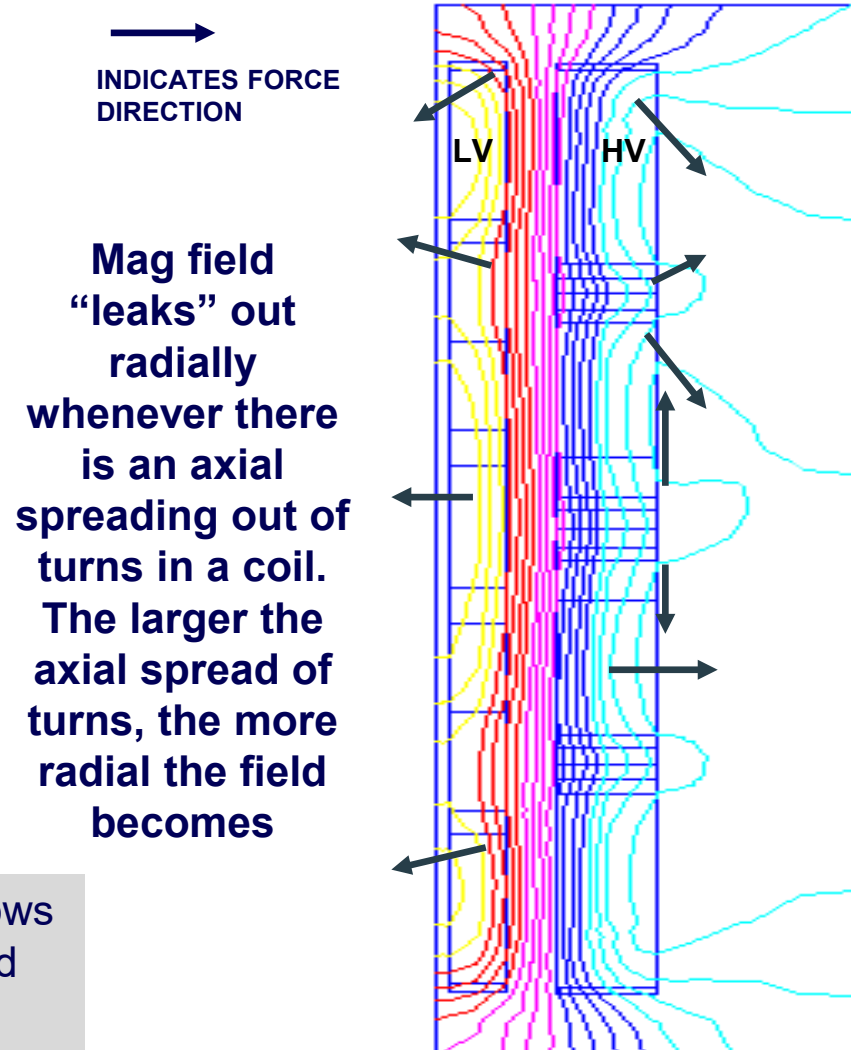
**Magnetic Field**

# Magnetic Forces Across the Coils

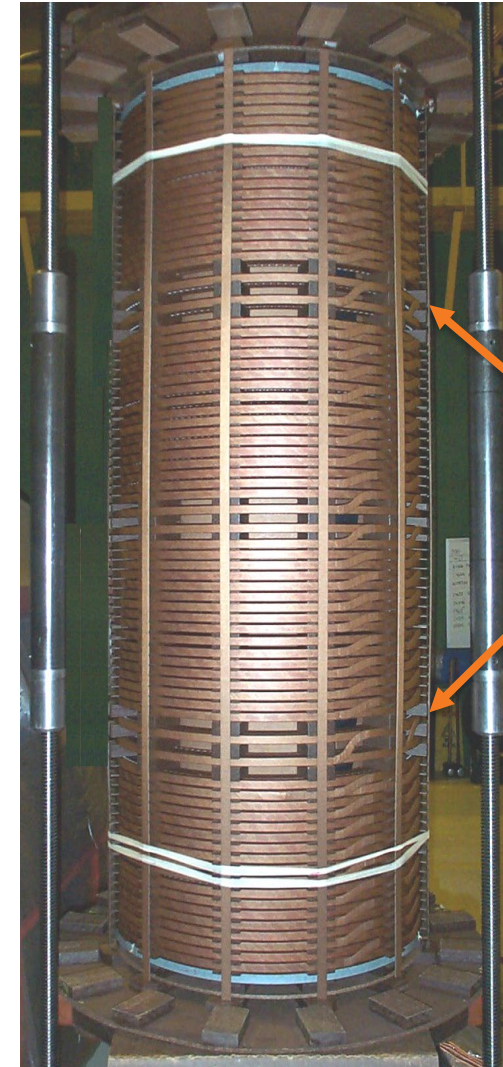


Note: The force arrows are acting in 3-D and perpendicular to the mag fields

# Pictorial of actual FEA field plots



Finite Element Analysis of  
Leakage Field Between Coils



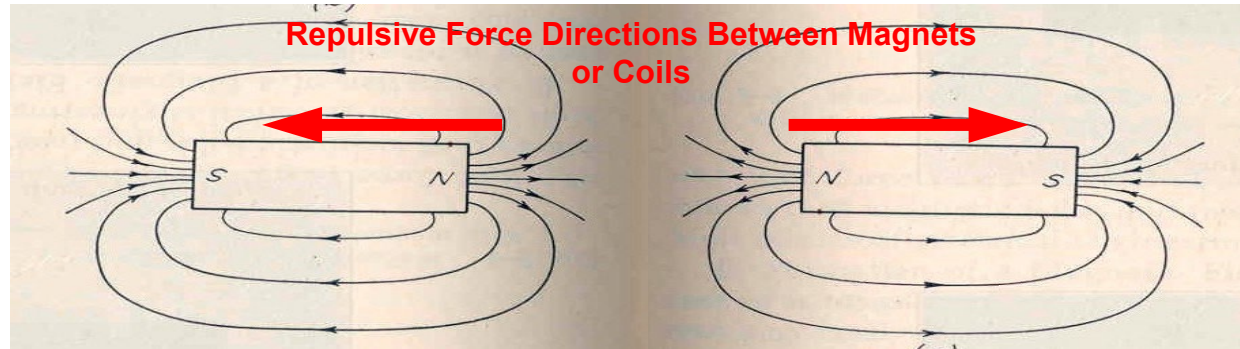
# Summary of what we discussed so far...

- Magnetic forces are produced whenever
  - You have current flowing thru a conductor, and
  - A leakage magnetic field also passes thru the conductor.
  - Resulting forces have a direction of 90 degrees to the direction of current through the conductor versus the direction of the leakage magnetic field around the conductor (left hand rule)
  - The leakage magnetic fields can pass thru conductors at any angle (3 dimensional)
  - Forces then are also 3 dimensional in nature



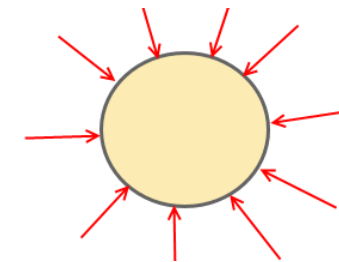
# Magnetic Forces

- A net magnetic force also results between two coils (i.e. HV to LV), because the two coils are essentially two huge electro-magnets that repel each other.

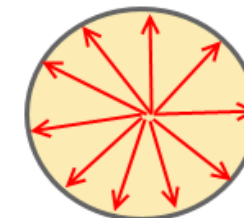


Summative force between these coils could be millions of pounds

- The inner coil experiences net inward radial “crushing” compressive forces
- The outer coil experiences net outward radial expanding type forces



LV coil



HV coil

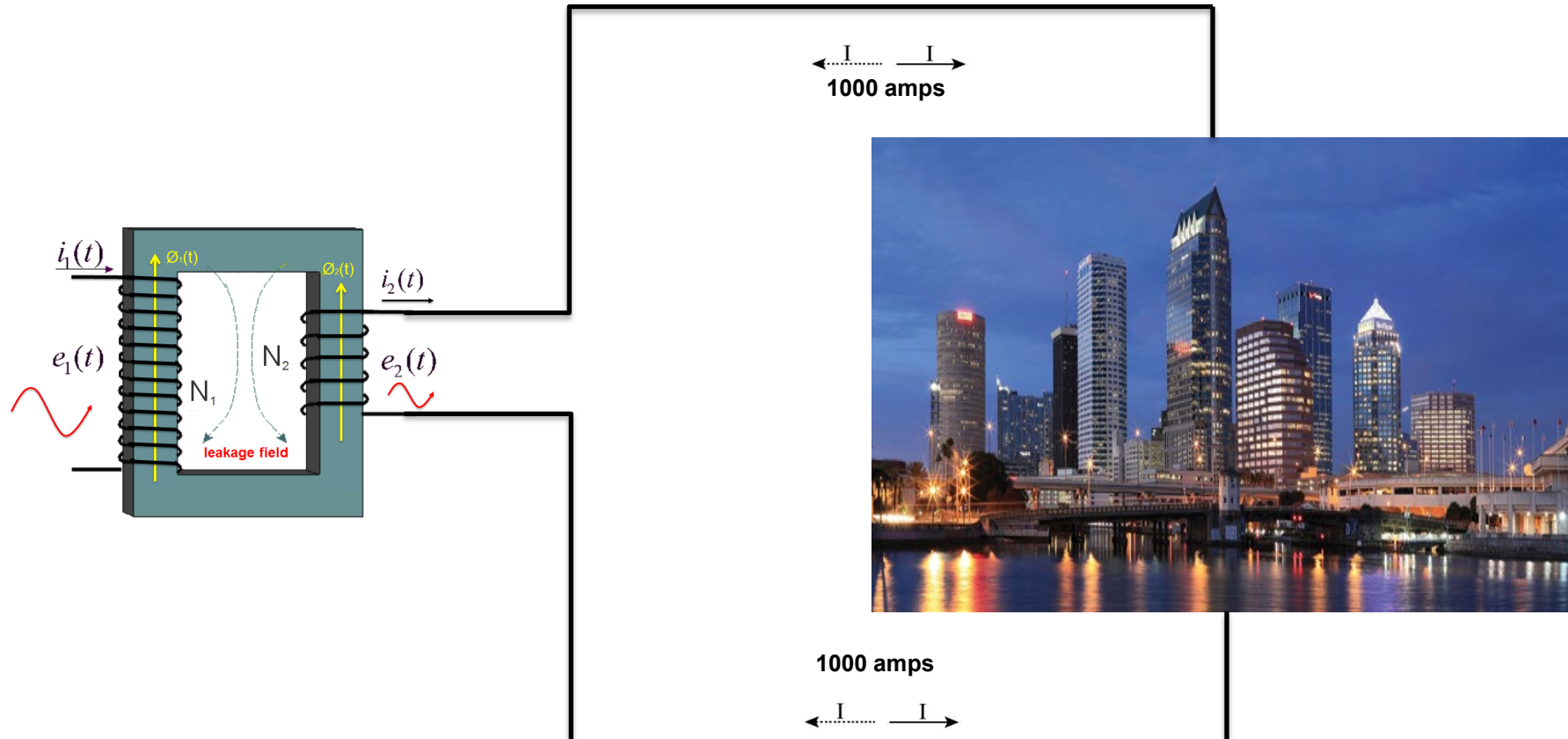
## Part 3 – Short Circuits (Faults):

- What are they?
- How do they happen?
- What do they do to my transformer?

# Normal Transformer Operation

## Normal Circuit

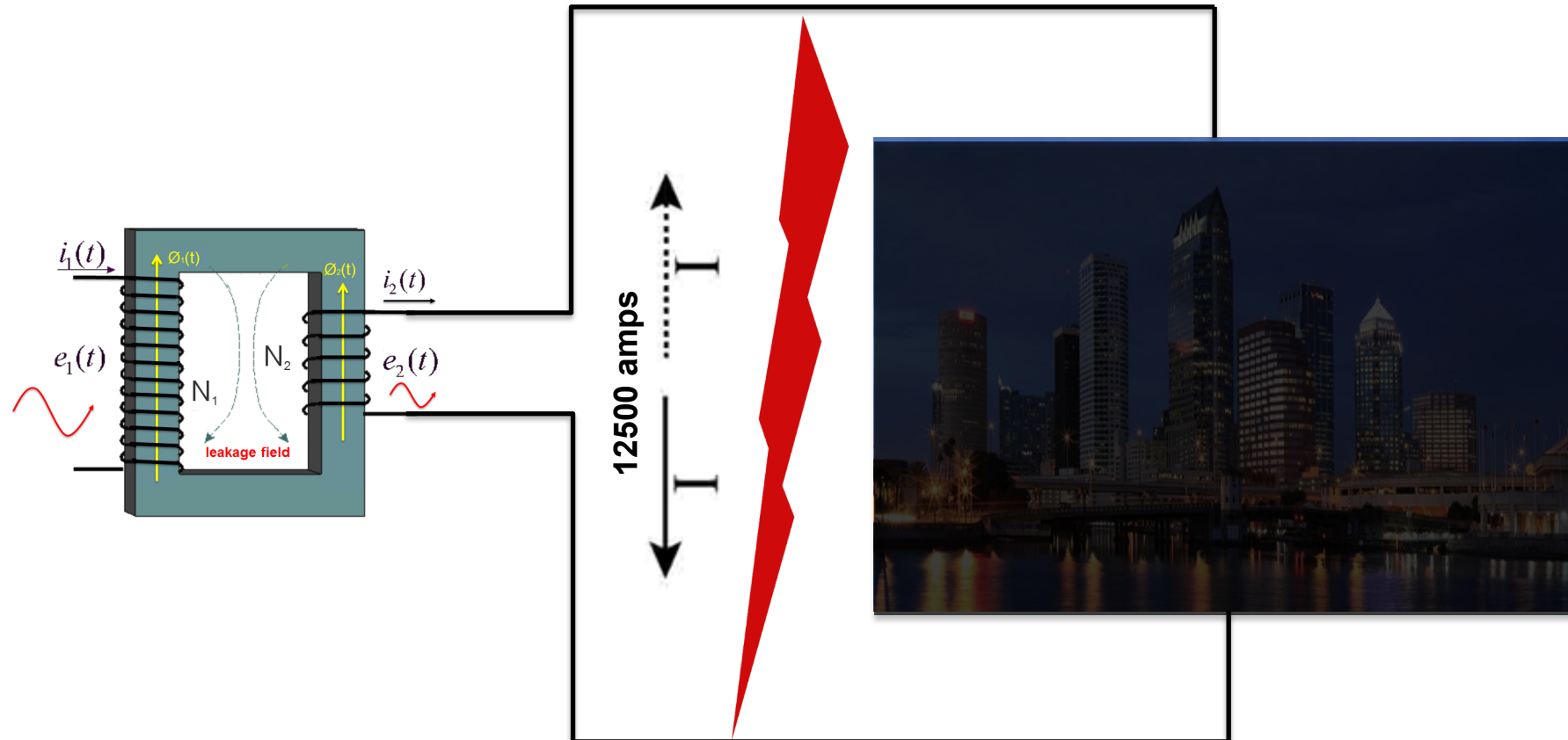
- An AC source supplies power to a given load (i.e. a city). A complete circuit has a source, with power entering a load and returning to the source. Amount of current that flows is directly related to the load on the transformer.



# What is a Fault?

## System Fault

- An un-intended “electrical connection” made between two energized components having different voltage potentials.
- Results in some (or all) of the current bypassing the intended load.
- Currents are typically very high due to low “fault impedance”



# Types of Faults (and how they happen)

## Basic Types of Faults in Power Systems

- Line-to-Ground (Most Common)
  - One or more conductors make “electrical” contact to ground
  - Example: Wildlife or Lightning. A lightning strike hits a line, then causes a flashover. The stroke between the line and ground causes ionization of the air (a conductive channel path to ground).



Lightning can reach 100 million to 1 billion volts, and generate up to a billion watts of power

# Types of Faults (*cont.*)

## Basic Types of Faults in Power Systems

- Line-to-Line
  - Two different phases come into direct or indirect contact with each other
  - Example: A bird with a large wingspan touches two conductors simultaneously and creates a conductive path between the two lines



# Types of Faults (*cont.*)

## Basic Types of Faults in Power Systems

- Double Line-to-ground
- Three Phase (least common)
  - Similar to Line-to-Line but when all three phases make contact with each other
  - Example: A falling tree on a transmission line creates a conductive path between all 3 lines and to ground



# Designing For Short Circuit

Section 7 of IEEE C57.12.00 addresses design requirements for short circuit

- Fault current magnitudes and their behavior over time (time durations, wave shapes, etc).
- Temperature limits of winding conductor after a fault
- Power system impedance that may be used to help limit fault current
- Short circuit test methods and how to analyze, inspect, etc.



# Example of How to Calculate SC Current

C57.12.00 Section 7 defines both symmetrical and asymmetrical current

## Symmetrical Current

$$I_{SC} = \frac{I_R}{Z_T + Z_S}$$

- $I_{sc}$  – symmetrical SC Current (A, rms)
- $I_r$  – rated current (A, rms)
- $Z_t$  – transformer impedance for same voltage tap and MVA as rated current ( $I_r$ )
- $Z_s$  – system impedance in per unit on the same MVA base for rated current ( $I_r$ )

## Asymmetrical Current

$$I_{SC}(pk\ asym) = K I_{SC}$$

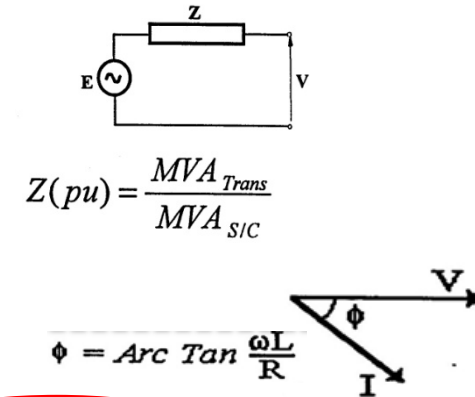
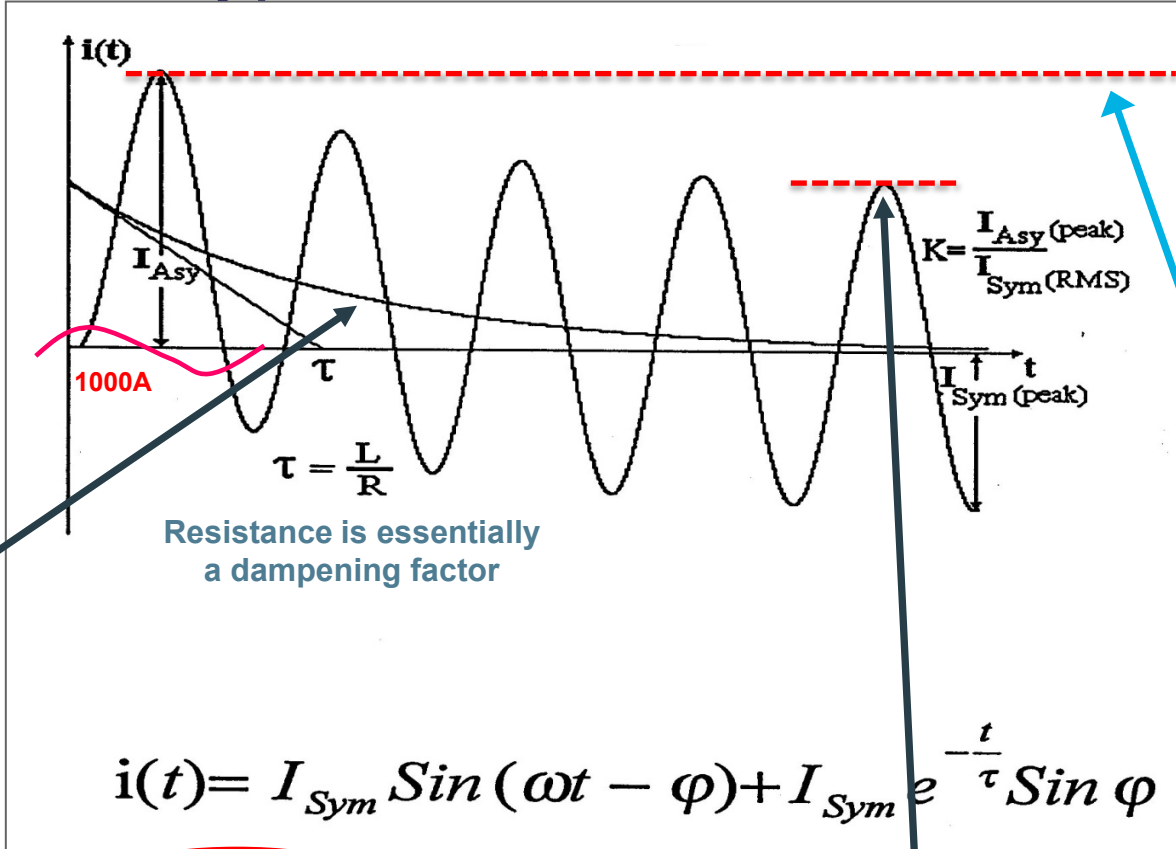
$$K = \left\{ 1 + \left[ e^{-\left(\phi + \frac{\pi}{2}\right)\frac{r}{x}} \right] \sin \phi \right\} \sqrt{2}$$

$\phi$  is arc tan ( $x/r$ ) (radians)

$e$  is the base of natural logarithm

$x/r$  is the ratio of effective ac reactance to resistance, both in ohms

# Waveform of Typical Fault Current Over Time



**Asymmetrical (Peak) current**

$$i(t) = I_{Sym} \sin(\omega t - \phi) + I_{Sym} e^{-\frac{t}{\tau}} \sin \phi$$

**Symmetrical (RMS) current**

$$I_{SC} = \frac{I_R}{\frac{Z_T + Z_S^*}{100}} \quad \text{OR} \quad I_{SC} = \frac{100}{\%Z} \times I_R$$

$$I_{SC} (\text{peak asym}) = K I_{SC} \text{ where}$$

$$K = \left\{ 1 + \epsilon^{-\left(\phi + \frac{\pi}{2}\right) \frac{r}{x}} \sin \phi \right\} \sqrt{2}, \text{ per unit}$$

$$\phi = \arctan \frac{x}{r}, \text{ radians}$$

(Symmetrical and Asymmetrical)

The fault current within a transformer will follow this typical exponential decay

Say Z were to be 8.0%, then: Isc would be 12.5x normal rated current

# Different Parts of the Formulas...

**ASSYM: MECHANICAL DAMAGE**

$e^{-t/\tau}$

The fault current entering a transformer will follow this typical exponential decay

$\phi = \text{Arc Tan } \frac{\omega L}{R}$

**4** Symmetrical

$K = \frac{I_{Asy}(\text{peak})}{I_{Sym}(\text{RMS})}$

**1** RATED AMPS

$\tau = \frac{L}{R}$

Resistance is essentially a dampening factor

**4** Symmetrical

**2** **3** DECAH PATTERN

**4** TO FIND ANY POINT IN THE TIMELINE

$i(t) = I_{Sym} \sin(\omega t - \phi) + I_{Sym} e^{-\frac{t}{\tau}} \sin \phi$

**4** Symmetrical (RMS) current

$$I_{SC} = \frac{I_R}{Z_T + Z_S^*} \quad \text{OR} \quad I_{SC} = 100 \times I_R \%Z$$

**4** Asymmetrical (Peak) current

$I_{SC}(\text{peak asym}) = K I_{SC}$  where

$K = 1 + \epsilon \left[ \sin \left( \phi + \frac{\pi}{2} \right) e^{-\frac{t}{\tau}} \right] \sqrt{2}$ , per unit

OFFSET VALUE MAINLY AFFECTED BY  $X/R$

$\phi = \arctan \frac{X}{R}$ , radians

FAULT TIME IN RADIANS WORSE CASE AT  $V=0$

CONVERT RMS  $\rightarrow$  PEAK

$\frac{1}{\tau} = R/X$

$Z_S = \frac{MVA_{Trans}}{MVA_{SIC}}$

$\tau = X/R$

**THIS FORMULA TAKES YOU RIGHT TO FIRST ASYMMETRICAL PEAK! POINT A**

**K RANGES  $\approx 1.5 - 2.83 \times I_{SC}$**

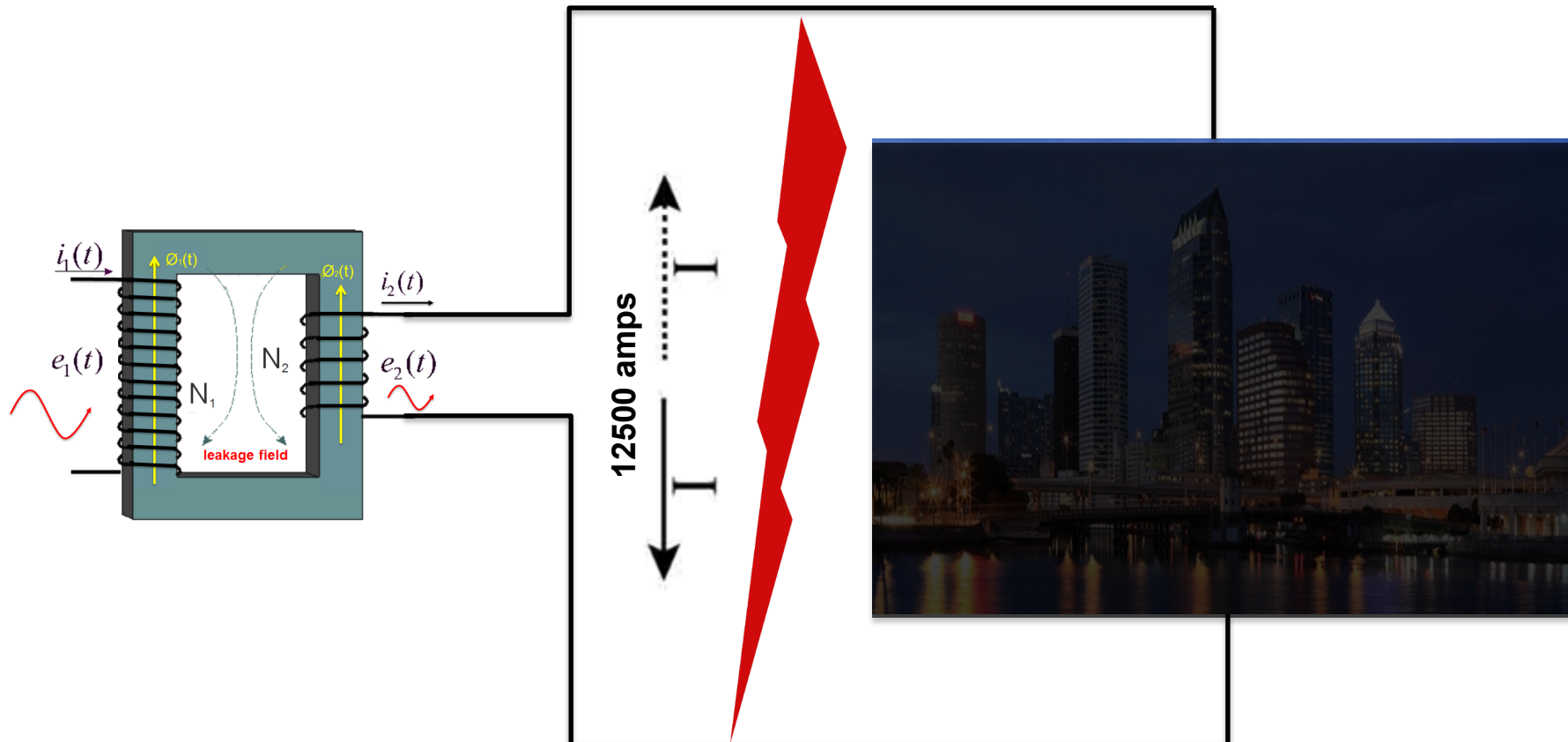
## Part 4 – Visualization of the Magnetic Forces:

- Axial Forces on Winding Conductors (and other components)
- Radial Forces on Winding Conductors
- Combination of Axial/Radial Forces

# Back to our Fault Condition...

## System Fault

- An un-intended “electrical connection” made between two energized components having different voltage potentials.
- Results in some (or all) of the current bypassing the intended load.
- Currents are typically very high due to low “fault impedance”



# Once the Fault Occurs...

- The transformer must source the current to feed the fault
- Very high currents (much higher than rated current) begin to flow in the transformer windings
- Very high temperatures can be generated in the winding conductors and paper insulation resulting from the high currents that flow.
- Very high magnetic forces can be generated within windings, leads, supporting structures and insulation systems.

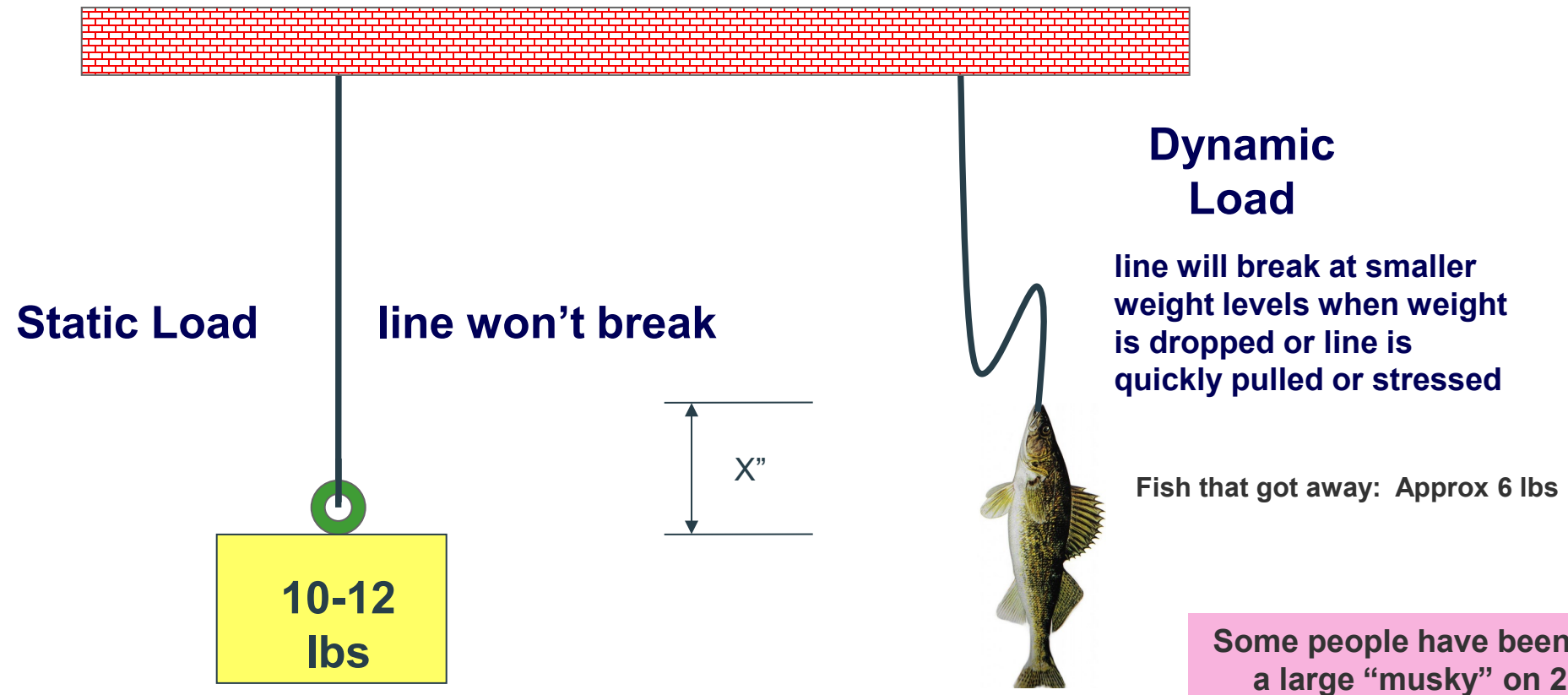
Short circuit forces are all acting in 3-D  
(combination of axial/radial/angular).

They can reach summative levels of up to 2+ million lbs,  
per phase, **INSTANTANEOUSLY!**

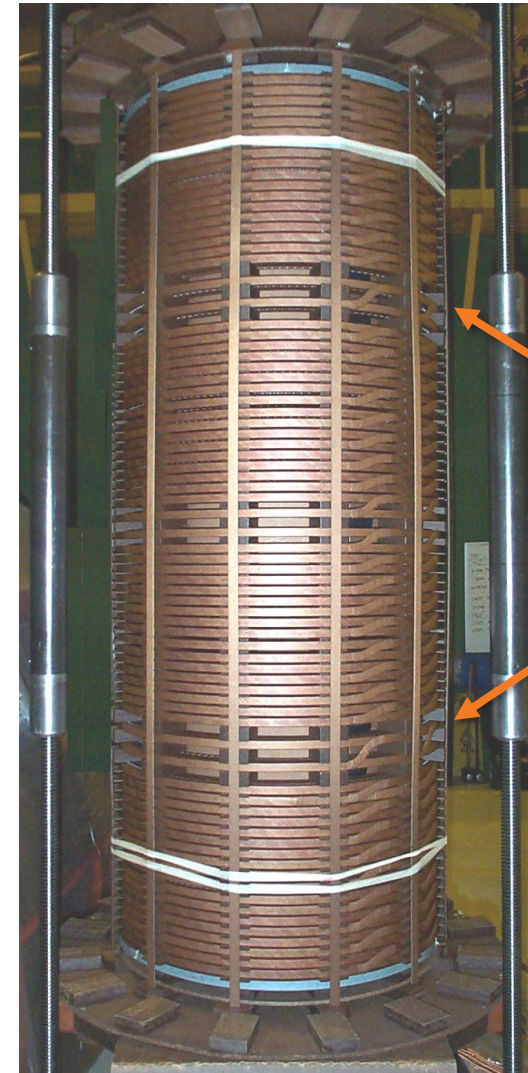
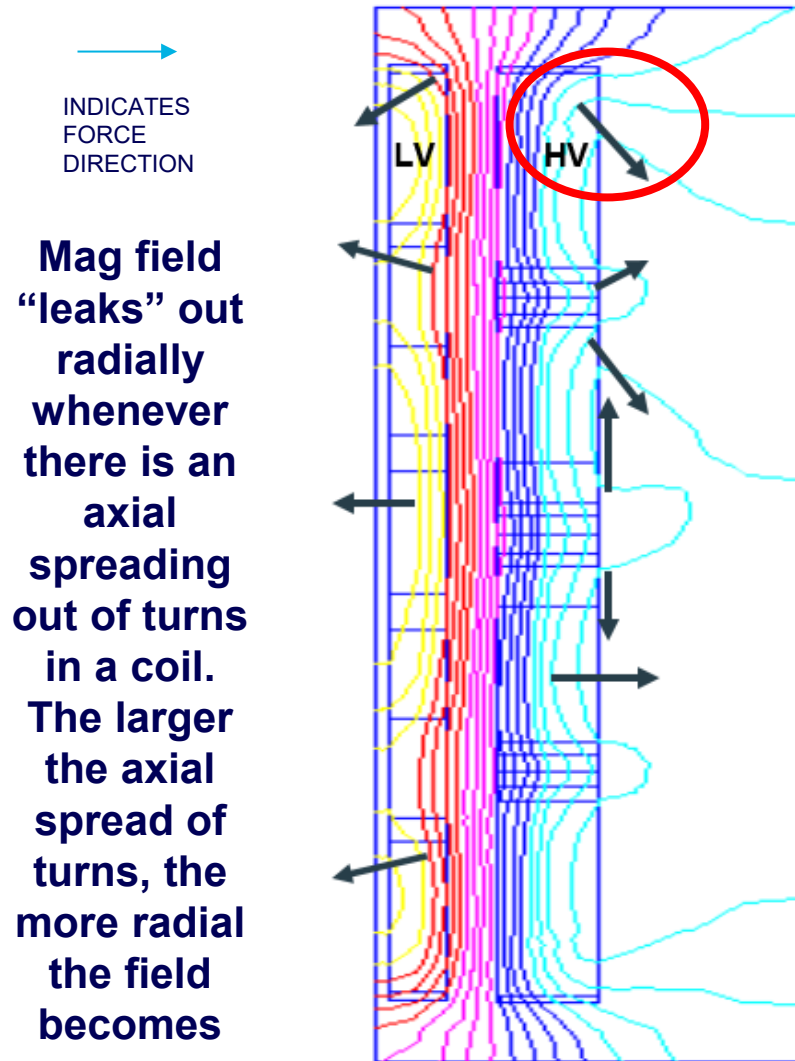
# Physics of Materials: Static vs Dynamic Stress

We know that: All materials behave differently under static (stationary) versus dynamic (moving) load conditions

Example using a weight suspended from a 10 lb test fishing line



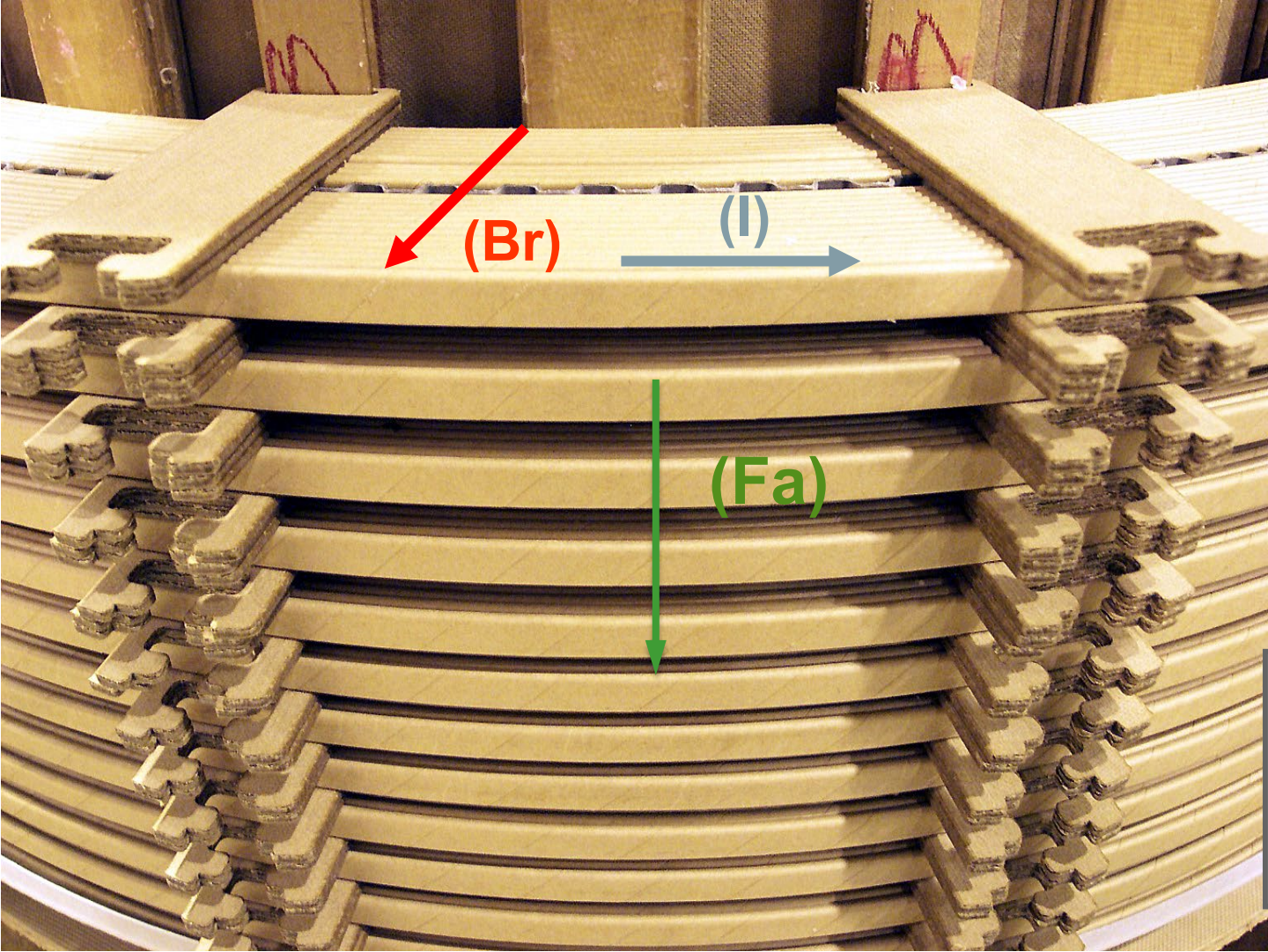
# Visualization of Magnetic Fields and Forces



Finite Element Analysis of Leakage Flux Between Coils



# Axial Forces - (Applying Left Hand Rule)



Current (I)

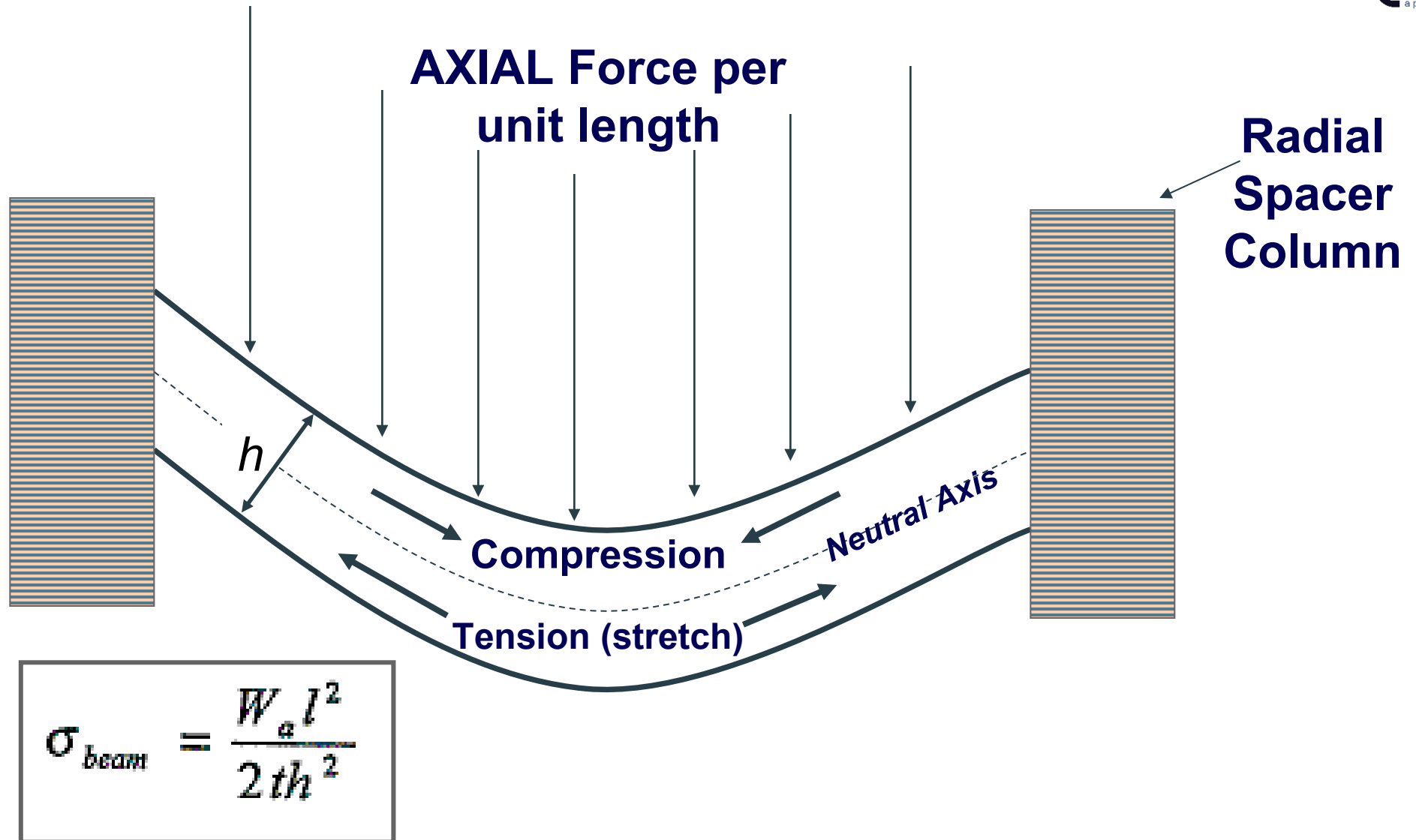
Flux (B)

Force (F)

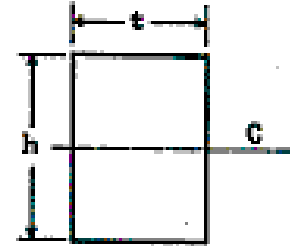
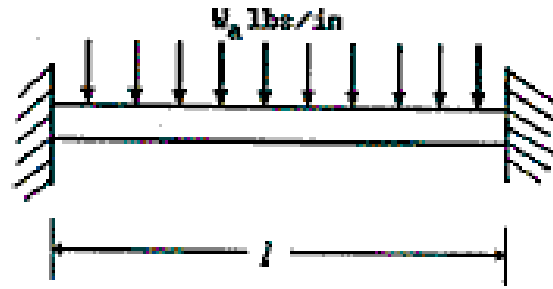
Length of beam:

$$l = \frac{2 \pi R_{OD}}{m} - W_b$$

# Beam Bending Under Load (elevation view)



# Beam Bending Stress



$$\sigma_{beam} = \frac{W_a l^2}{2th^2}$$

where:

- $R_{OD}$  = Winding O.D. (inches)
- $W_{ks}$  = Keyspacer Width (inches)
- $m$  = Number of Key Spacer Strings
- $F_{max}$  = Maximum Force on a Disk or Conductor (lbs)

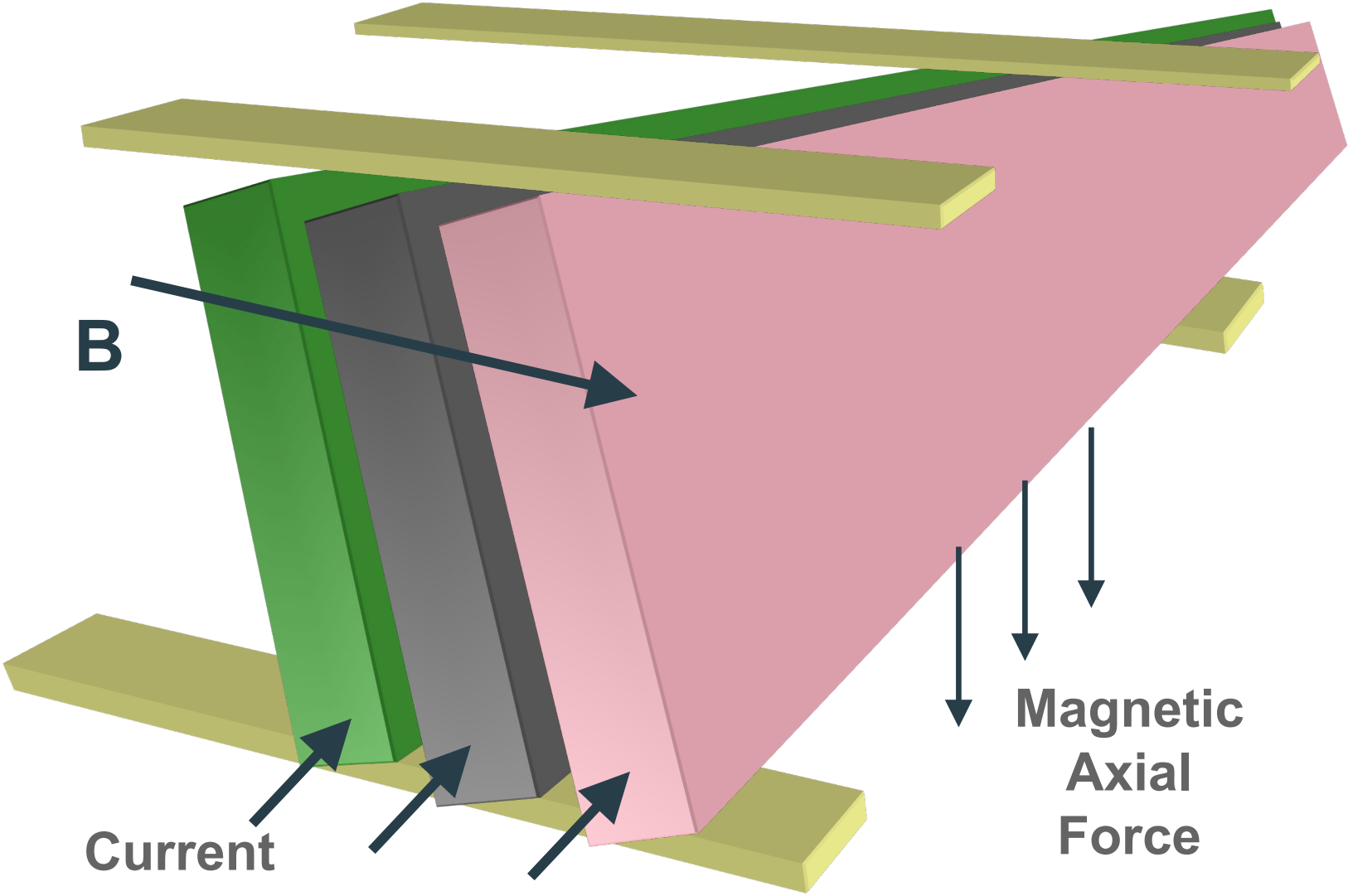
**Length of beam:**

$$l = \frac{2\pi R_{OD}}{m} - W_{ks}$$

**Linear Load:**

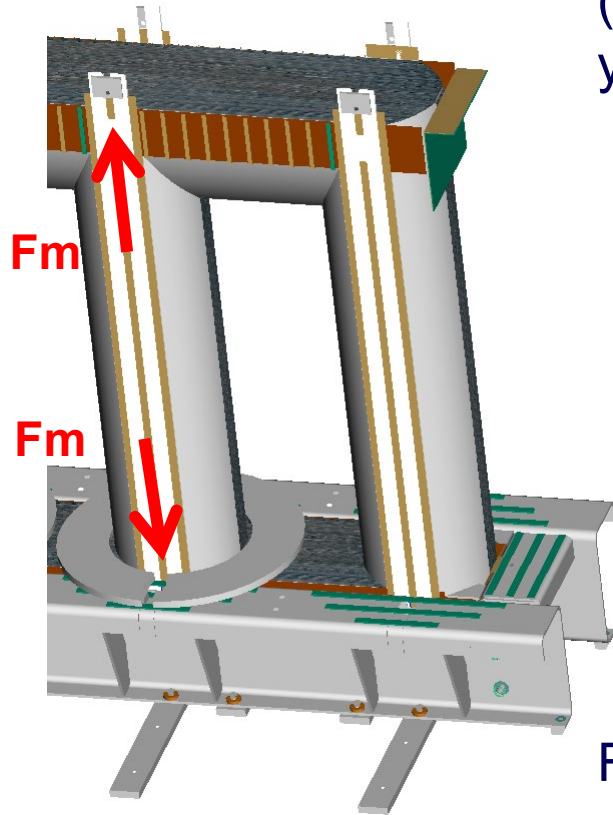
$$W_a = \frac{F_{max}}{l}$$

# Conductor Tipping/Tilting



# Stress in Tie Bars (Verticals)

The minimum cross-sectional area of the tie bar ( $A_{tb}$ ) is determined by the force applied and the yield point of the tie bar material.



$$A_{tb} = \frac{F_m / 2}{70,000}$$

Yield Strength of Tie Bar = 100,000 PSI

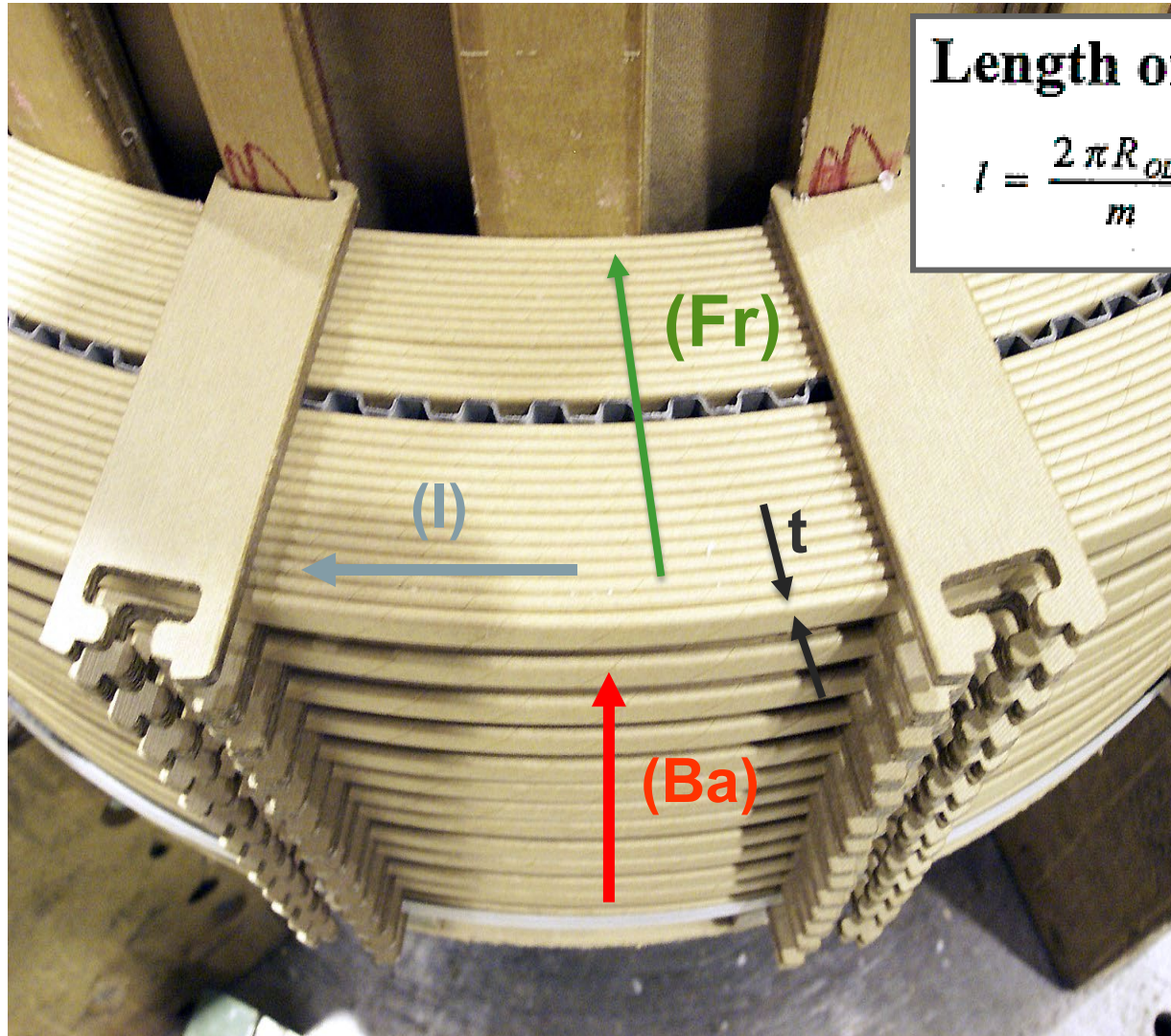
70% of yield = 70,000 PSI

$F_m/2$  to get minimum area per tie bar (2 per phase)

$F_m$  is the larger of:

- maximum axial short circuit force (PSI)
- maximum winding sizing per phase (PSI)

# (Inward) Radial Forces – Buckling (inner coil)



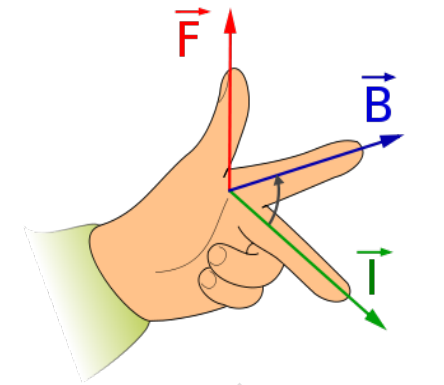
**Length of beam:**

$$l = \frac{2 \pi R_{OD}}{m} - W_{kr}$$

Current (I)

Flux (B)

Force (F)

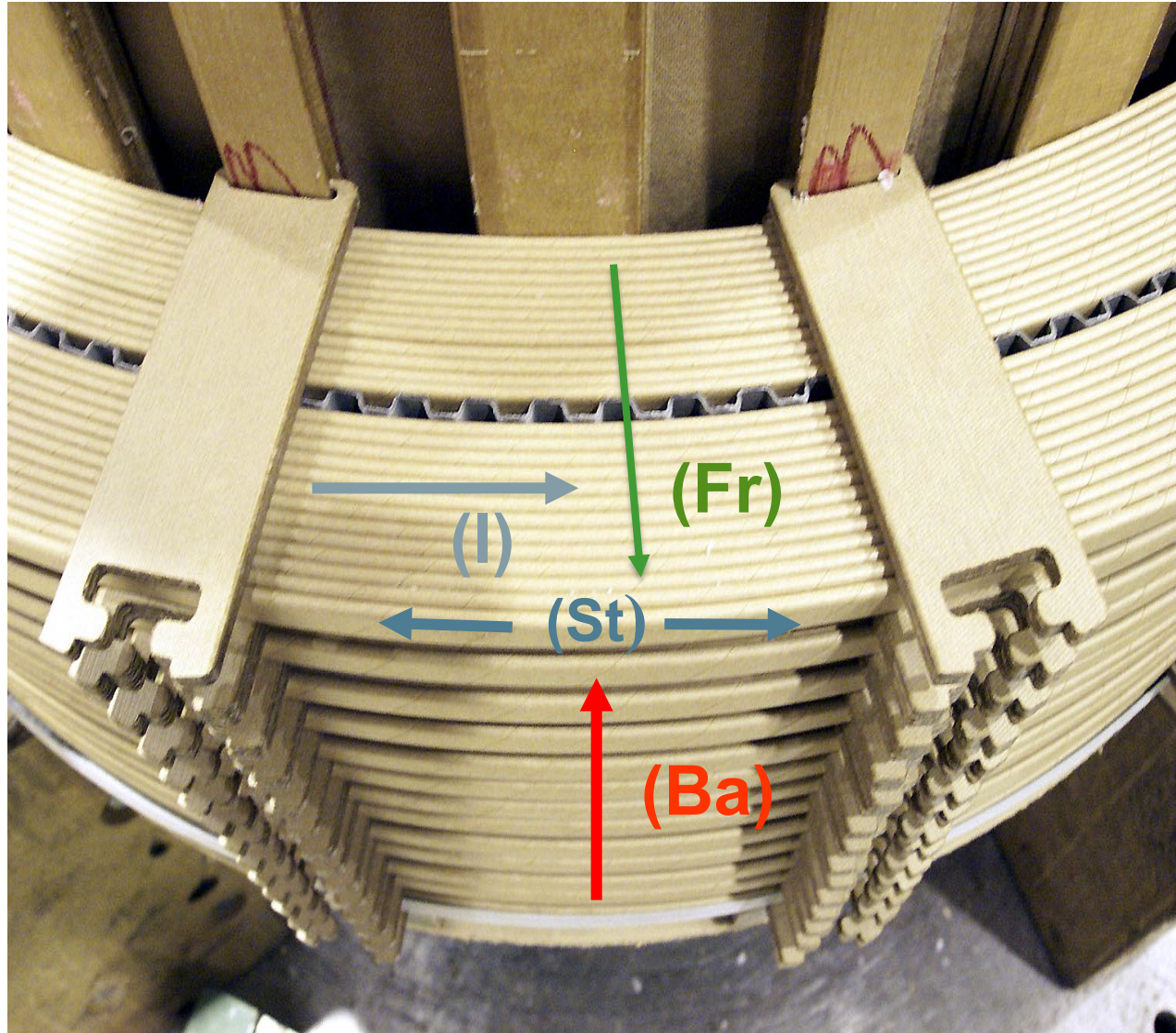


Left-Hand Rule

# Buckling Photo - Inner Winding Forced Into Failure in a Laboratory Setting...



# OUTWARD Radial Forces – Hoop Stress (outer coil)

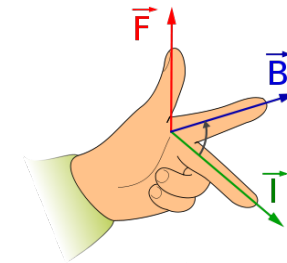


Current ( $I$ )

Flux ( $B$ )

Force ( $F$ )

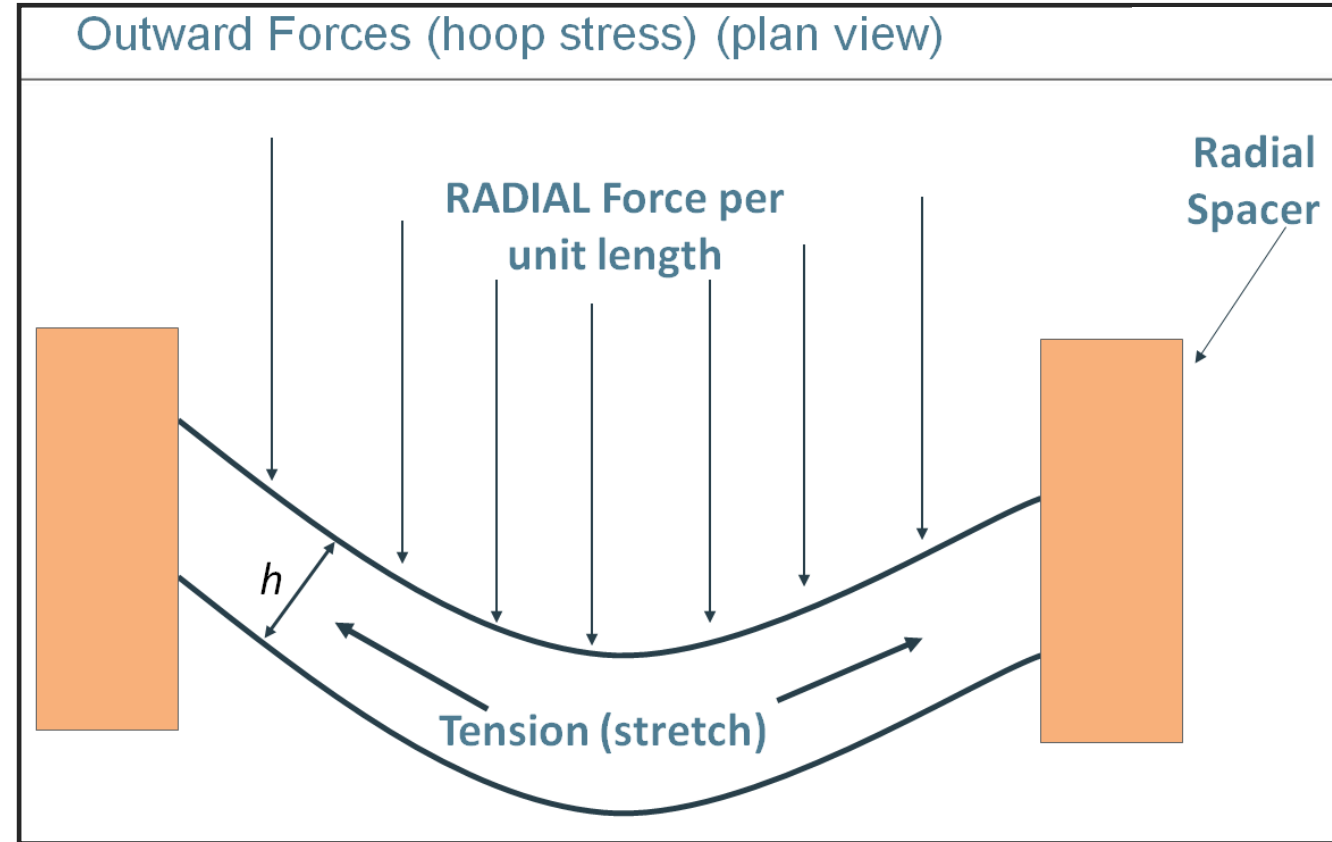
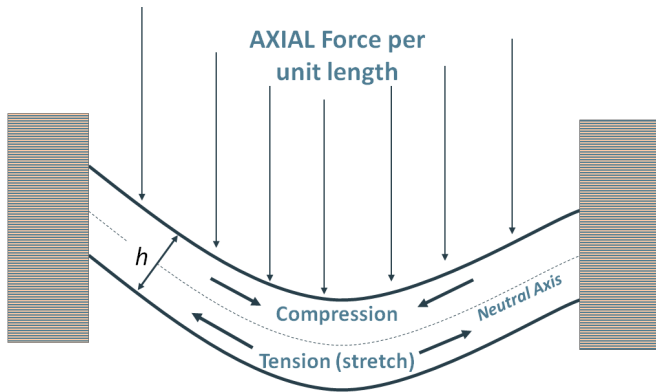
Tensile  
Stress ( $St$ )



Left-Hand Rule



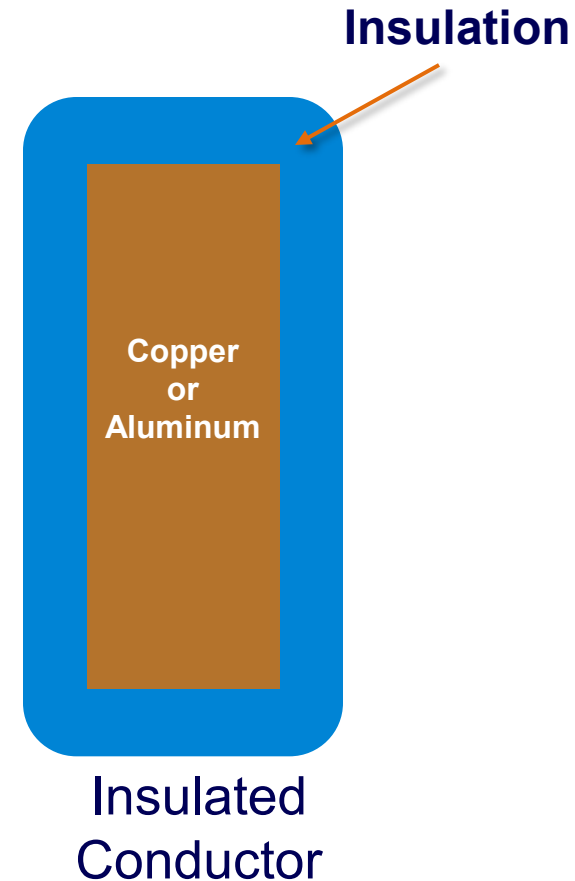
# Outward Forces (hoop stress) - Outward Radial Force exerts Tensile Stress only



**No neutral axis**

# Winding Temperature During a Short Circuit

- Calculated on basis that all heat is stored (heats up too quickly to radiate heat to equilibrium)
- Temperature not to exceed
  - 250°C for copper
  - 200°C for EC grade aluminum
- Method defined on IEEE C57.12.00-2000 section 7.4.



# Winding Temperature During a Short Circuit

Approximate method:

$$T_f = \frac{(S_{\Delta k})^2 t}{K_m} + T_{OR} + T_a$$

$T_f$  = final winding temperature at end of a short circuit (°C)

$T_{OR}$  = maximum top liquid temperature rise over ambient temperature (°C)

$T_a$  = ambient temperature (°C)

$S_{\Delta k}$  = winding current density at symmetrical short circuit current (W/dm<sup>2</sup>)

$t$  = short circuit duration (s).

$K_m$  = 156 for copper / 73 for EC grade aluminum

## Part 5 – Calculation Example:

- Calculate short circuit current and asymmetrical offset factor

# Back to our formulas again....

**ASYM: MECHANICAL DAMAGE**

**ASYMMETRICAL (Peak) current**

The fault current entering a transformer will follow this typical exponential decay

$Z_S = \frac{MVA_{Trans}}{MVA_{SC}}$

$\tau = \frac{L}{R}$   
Resistance is essentially a dampening factor

$\phi = \text{Arc Tan } \frac{\omega L}{R}$

$K = \frac{I_{Asy}(\text{peak})}{I_{Sym}(\text{RMS})}$

**TO FIND ANY POINT IN THE TIMELINE**

$i(t) = I_{Sym} \sin(\omega t - \phi) + I_{Sym} e^{-\frac{t}{\tau}} \sin \phi$

**Symmetrical (RMS) current**

$I_{SC} = \frac{I_R}{Z_T + Z_S^*}$  OR  $I_{SC} = \frac{100}{\%Z} \times I_R$

**K RANGES  $\approx 1.5 - 2.83 \times I_{SC}$**

**Asymmetrical (Peak) current**

$I_{SC}(\text{peak asym}) = K I_{SC}$  where

$K = \left\{ 1 + \epsilon \left[ \frac{1 + \cos(\phi + \frac{\pi}{2})}{1 - \cos(\phi + \frac{\pi}{2})} \right] \right\} \sqrt{2}$ , per unit

OFFSET VALUE MAINLY AFFECTED BY  $X/R$

$\phi = \arctan \frac{X}{R}$ , radians

FAULT TIME IN RADIANS WORSE CASE AT  $V=0$

$\frac{1}{\tau} = R/X$

**THIS FORMULA TAKES YOU RIGHT TO FIRST ASYMMETRICAL PEAK! POINT A**

# Example of How to Calculate SC Current

Assume we have a transformer with a 69kV primary and the following known data:

Transformer MVA = 30 MVA base

Rated amps on LV (@ 30 MVA) = 1000 amps

Tested load loss @ 30 MVA: 72.0 kw

Tested impedance @ 30 MVA: 8.0% (= 0.8 p.u.)

To find  $I_{sc}$ (RMS symmetrical) and  $I_{sc}$ (Peak Asym), we must perform 3 steps in the following order:

1. Determine  $I_{sc}$  (RMS symmetrical)
2. Determine offset (asymmetrical) “K” factor
3. Apply derived data from 1. and 2. to determine peak offset asymmetrical amps.

Next 

# Example of How to Calculate SC Current

## STEP 1: Find $I_{SC}$ (RMS symmetrical)

Note:  $Z_T$  and  $Z_s$  are in p.u.

$$I_{SC} = \frac{I_R}{Z_T + Z_S}$$

$$I_{SC} = \frac{1000}{0.08 + 0} = 12,500A$$

OR, using the other formula ...

$$I_{SC} = \frac{100}{8\% + 0\%} \times I_{\text{rated}}$$

$$I_{SC} = \frac{100}{8\% + 0\%} \times 1000A = 12,500A$$

Symmetrical Current without  $Z_s$

Symmetrical Current with  $Z_s$

$$I_{SC} = \frac{I_R}{Z_T + Z_S}$$

$$I_{SC} = \frac{1000}{0.08 + Z_s}$$

$$Z_s = \frac{MVA_T}{MVA_S} = \frac{30}{9800} = 0.31\%$$

$$I_{SC} = \frac{1000}{0.08 + 0.0031} = 12,034 A$$

Note:  $Z_s$  is derived from C57.12.00-2010 Table 15 if not specified from customer.

Difference (with vs without  $Z_s$ ) is almost 500A or 4%

Next 

# Example of How to Calculate SC Current

## Step 2: Determine the “K” factor:

To find “K” factor, we need to determine %R and X/R ratio...

$$K = \left\{ 1 + \left[ e^{-\left(\phi + \frac{\pi}{2}\right)\frac{r}{x}} \right] \sin \phi \right\} \sqrt{2}$$

### 1. Find %R

$$\%R = 100x \frac{\text{Load Loss (kW)}}{KVA_T} = \frac{100x72}{30,000} = 0.24\%$$

### 2. Find X/R

$$\frac{X}{R} = \frac{Z_T}{\%R} = \frac{8\%}{0.24\%} = 33.33$$

Plug these values into next equation



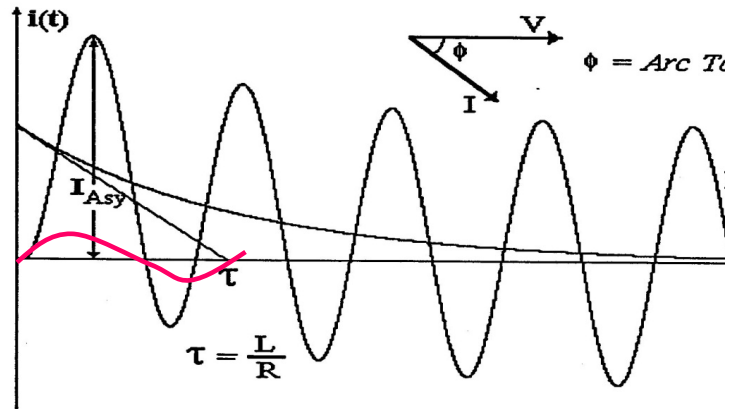
# Example of How to Calculate SC Current

Step 2 (continued): Determine the “K” factor:

$$K = \left\{ 1 + \left[ e^{-\left(\phi + \frac{\pi}{2}\right) \frac{r}{x}} \right] \sin \phi \right\} \sqrt{2}$$

$$K = \left\{ 1 + \left[ e^{-\left(\tan^{-1}(33.33) + \frac{\pi}{2}\right) * \frac{1}{33.33}} \right] * \sin(\tan^{-1}(33.33)) \right\} * \sqrt{2}$$

$$K = 2.702$$



C57.12.00-2010 Table 14

$x/r$	$K$
1000.00	2.824
500.00	2.820
333.00	2.815
250.00	2.811
200.00	2.806
167.00	2.802
143.00	2.798
125.00	2.793
111.00	2.789
100.00	2.785
50.00	2.743
33.30	2.702

# Example of How to Calculate SC Current

## Step 3: Determine the $I_{sc}$ (Peak Asymmetrical):

Since  $I_{sc}(\text{peak asym}) = K \times I_{sc}(\text{RMS symmetrical})$

then ...

$$I_{sc}(\text{peak asym}) = 2.702 \times 12,500 \text{ amps} = \underline{33,750 \text{ amps}}$$

**FYI: Since  $F \propto I^2$**

**The Txf forces will see  $(33750 \text{ amps} / 1000 \text{ amps})^2 = (33.75)^2 = 1140 \times$  normal forces**

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# Questions



## Contact

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